November 18, 2019

# 6101 E. **CABALLO**

Town of Paradise Valley, AZ

Prepared for:

**DK Real Estate Holdings, LLC** 

130 N. 35th Avenue Phoenix, Arizona 85009

Prepared by:

Coe & Van Loo Consultants, Inc.

4550 N 12th Street Phoenix, AZ 85014

602.264.6831



Job # 1-01-0326801

# DRAINAGE REPORT FOR 6101 E. CABALLO LANE

TOWN OF PARADISE VALLEY, ARIZONA

November 18, 2019

Prepared for:

DK Real Estate Holdings, LLC 130 N. 35<sup>TH</sup> Avenue Phoenix, AZ 85009 (602) 254-6978

Prepared by:

Coe & Van Loo Consultants, Inc. 4550 N. 12th Street Phoenix, AZ 85014 (602) 264-6831

CVL Job Number: 1.01.0326801



Approved By:		
	Town Engineer	Date

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# **Plates**

Plate 1 Offsite Drainage Map

Plate 2 HEC-RAS Map

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Sheet 1 Existing Condition Plan View
Sheet 2 Proposed Condition Plan View

Sheet 3 Cross Section View





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# 1.0 Introduction

# **1.1 SCOPE**

Coe & Van Loo Consultants, Inc. (CVL) has been contracted by DK Real Estate Holding, LLC to provide engineering services to evaluate offsite drainage conditions at 6101 E. Caballo Lane, herein referred to as the site. Please see Figure 1 for the Vicinity Map. The purpose of this report is to provide drainage analysis to evaluate peak flows affecting the site.

This report is focused on providing evaluation and analyses for the 100-year frequency flood. The scope of this assessment does not include, neither did CVL's client request that, evaluation of storm-water runoff resulting from events exceeding the 100-year storm. Hence, it should be noted that a storm event exceeding the 100-year frequency may cause or create the risk of greater flood impact than is addressed and presented in this assessment.

The procedures used herein are derived from, and performed with, currently accepted engineering methodologies and practices. Additionally, the criteria for this evaluation are designed to conform to currently applicable ordinances, regulations and policies as set forth by the Town of Paradise Valley and Maricopa County.

### 1.2 SITE DESCRIPTION

The site is a residential lot containing two houses and a tennis court and is approximately 2.49 acres in size. The site is bisected by Cherokee Wash. Offsite flows pass through the site and then into Indian Bend Wash. The site is bounded by Caballo Lane on the north, Morning Glory Road on the west, Caballo Drive on the south and two residential lots to the east (see Figure 1 for a Vicinity and Location Map). The site is located in Section 33, Township 3 North, Range 4 East of the Gila and Salt River Base and Meridian, Maricopa County, Arizona.

# 1.3 REGULATORY JURISDICTION

Site improvements will be designed to meet requirements in the Town of Paradise Valley Engineering Storm Drain Design Manual [1], and in accordance with analysis procedures contained the Drainage Design Manuals for Maricopa County, Arizona, Volume I, Hydrology [2], Volume II, Hydraulics [3], and Drainage Policies and Standards Manual for Maricopa County, Arizona [4].



# 2.0 Hydrologic Setting

The Cherokee Wash watershed extends from near Tatum Boulevard to Indian Bend Wash. Hydrologic analysis used for this report was prepared previously for the Doubletree Ranch Road Drainage Improvement Project (Study) (see Appendix A). The site slopes generally northeast at 0.1% slope. Cherokee Wash enters the site from the west, passes through the middle of the site, and then exits to the northeast.

# 3.0 FEMA FLOODPLAIN CLASSIFICATION

The Maricopa County, Arizona and Unincorporated Areas Flood Insurance Rate Map (FIRM), panel number 04013C1755L, Map Revised October 16, 2013 [5], indicates the site falls within Zone "X."

Zone "X" is defined by FEMA as:

"Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood."

Refer to Figure 2 for a copy of the Flood Insurance Rate Map (FIRM).

# 4.0 OFF-SITE DRAINAGE

# 4.1 OFF-SITE HYDROLOGY

Flow into Cherokee Wash was taken from the Doubletree Ranch Road Drainage Improvement Project Final Design Study Report (see Appendix A). The 100-year peak flow within Cherokee Wash at 56<sup>th</sup> Street is 1813 cfs. Based on descriptions and results from the Study, not all of the 100-year storm flows can reach the site. Additionally, the report determines that the design of the box culvert at 56<sup>th</sup> Street was for the 10-year event.

# 4.2 Off-site Runoff Between 56<sup>th</sup> Street and the Site

In order to determine peak flows arriving at the site, flow patterning from the LIBW ADMS 2D modeling results was reviewed. This review helped to identify potential flow-split locations. Flow split locations were verified based on site visits and existing drainage infrastructure at 56<sup>th</sup> Street and east to the site. These are shown on the Drainage Map (see Plate 1). Flow-split calculations were prepared using



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CulvertMaster v.3.3 and FlowMaster V8i. The culvert size at Cherokee Wash and 56<sup>th</sup> Street was obtained from the Doubletree Report. Culvert calculation with roadway overtopping (location A1) is located in Appendix B. Results indicate 871 cfs remains in the wash downstream of 56<sup>th</sup> Street (see Plate 1). Appendix C contains calculations for flow-splits (A2 through A6) east of 56<sup>th</sup> street which are strategically located to determine flows that do not recombine with Cherokee Wash. Accounting for flow diversions from Cherokee Wash, a peak flow of 378 cfs enters the site (see Plate 1).

### 4.3 HEC-RAS ANALYSIS AT THE SITE

The existing condition of the wash was analyzed using HEC-RAS v5.0.7 to determine water surface elevations through the site. Geometric data for the model was obtained from site survey. Layout of cross-sections starts upstream and downstream of the western and eastern boundaries of the site. Results show the maximum water surface elevation is 1328.34 feet. However, the finished floor elevation for both structures on the site is 1329.40 feet, which allows for a minimum of 1.06 feet of freeboard. Manning's 'n' values were based on site inspection of the channel and Table 7.6, (B.a.1. and B.b.2) of the Drainage Design Manual for Maricopa County Volume 2-Hydraulics [3]. This corresponds to "Clean, after weathering" for the main channel (0.022) and "Stony bottom" for banks (0.035).

A proposed condition wash was also analyzed using HEC-RASv5.0.7. The proposed condition model was developed in order to establish a better-defined drainage easement for the wash in the event of a lot split. The proposed conditions model uses maximum side slopes of 4:1 and maintains the same Manning's n value as the existing condition channel. The proposed condition model shows that the flow is able to be contained within a narrower channel without increasing water surface elevations.

See Appendix D for HEC-RAS output of the existing and proposed models and see Plate2 for HEC-RAS map. Additionally, the Drainage Easement Exhibit shows a comparison of the existing and proposed conditions floodplain.



# 5.0 SUMMARY AND CONCLUSIONS

- 1. Off-site peak flows from Cherokee Wash are conveyed through the site.
- 2. No modifications or improvements are needed as the existing channel has over one foot of freeboard to the finished floor of the house.
- 3. A proposed condition HEC-RAS model demonstrates the channel can be narrowed while maintaining a foot of freeboard relative to the finished floor elevation.
- 4. According to the FIRM panel number 04013C1755L, Map Revised: October 16, 2013, the site is located within a Zone "X".
- Analysis of Cherokee Wash through the site is based on generally accepted engineering practices and is in accordance with local jurisdictional requirements.

# **6.0 REFERENCES**

- [1] Town of Paradise Valley, "Storm Drain Design Manual," June, 2018.
- [2] Flood Control District of Maricopa County, "Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology," December 14, 2018.
- [3] Flood Control District of Maricopa County, Arizona, "Draft Drainage Design Manual for Maricopa County, Volume II, Hydraulics," December 14, 2018.
- [4] Flood Control District of Maricopa County, "Drainage Policies and Standards," August 22, 2018.
- [5] Federal Emergency Management Agency (FEMA), "National Flood Insurance Program, Flood Insurance Rate Map, Maricopa County, Arizona and Incorporated Areas, Panel Numbers 04013C1755L," Revised October 16, 2013.

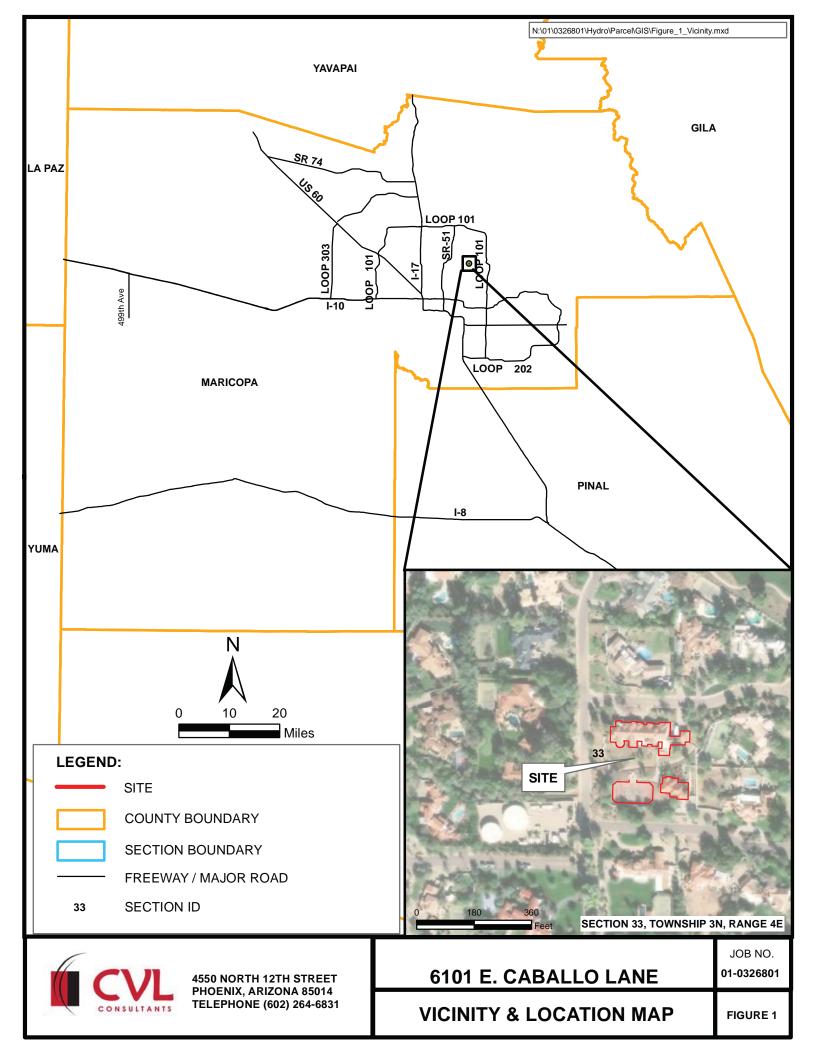


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# **FIGURES**







# **APPENDICES**



# **APPENDIX A**

# Doubletree Ranch Road Drainage Improvement Project Final Design Study Report



# DOUBLETREE RANCH ROAD DRAINAGE IMPROVEMENT PROJECT - FINAL DESIGN STUDY REPORT (FCD 97-32)

# Prepared for:

# FLOOD CONTROL DISTRICT OF MARICOPA COUNTY

2801 West Durango Phoenix, Arizona 85009

# Prepared by:

# **DIBBLE & ASSOCIATES, CONSULTING ENGINEERS**

2633 East Indian School Road, #401 Phoenix, Arizona 85016 (602) 957-1155



subdivision drainageways to the IBW. Historically, runoff emanating from the mountains traveled overland through numerous small washes to the IBW. Developments have altered many of these flow paths due to parcel subdivision, landscaping and block wall construction. As a result, Doubletree Ranch Road becomes a major water carrier and is impassable to traffic. Many homes experience flooding during frequent rainfall events and standing water in streets isolates the community. In particular, Cherokee Elementary School at 56<sup>th</sup> Street, south of Doubletree Ranch Road is isolated during all but the smallest rainfall events.

Computed peak discharges at key concentration points are summarized in **Table 1** for the 10-and 100-year storms for existing conditions and with the recommended 10-year storm drain system in place. The 100-year flows with storm drain are residual overland flow values. The HEC-1 summary output for the 10-, and 100-year models is contained in the **Appendix**.

Table 1

Location	Existing (	Conditions	10-yr Storm Drain	
	10-yr	100-yr	10-yr	100-yr
	Overland	Overland	with Storm Drain	Residual overland flow
Tatum Blvd @ Doubletree Ranch Rd.	284	686	284	402
52 <sup>nd</sup> St. @ Butler Drive	92	220	92	128
52 <sup>nd</sup> St. @ Doubletree Ranch Rd./South	N/A	515	209	215
Berneil Wash @ 52 <sup>nd</sup> St.	135	326	135	191
52 <sup>nd</sup> St. @ Doubletree Ranch Rd./North	2	5	135	5
Doubletree Ranch Rd. @ 52 <sup>nd</sup> St.	295	N/A	627	409
Cherokee Wash @ 56 <sup>th</sup> St.	789	1813	789	1813
56 <sup>th</sup> St. @ Cherokee Wash	108	318	184	79
56 <sup>th</sup> St. @ Doubletree Ranch Rd.	145	395	219	120
Doubletree Ranch Rd. @ 56 <sup>th</sup> St.	726	2025	909	933
Doubletree Ranch Rd. @ IBW	925	2145	954	1432

Note: Decreasing flows going downstream include diversions into the storm drain.

within Berneil Wash and divert it south along 52<sup>nd</sup> Street to the Doubletree Ranch Road Trunkline.

# (D) 56<sup>th</sup> Street Lateral

The 60-inch 56<sup>th</sup> Street Lateral will collect runoff at Cherokee Wash and convey it north along 56<sup>th</sup> Street to the Doubletree Ranch Road Trunkline. The inlet at Cherokee Wash is designed to intercept the portion of the 10-year discharge in Cherokee Wash that exceeds the channel capacity. The intent is to fully utilize the existing channel capacity and only provide storm drain capacity for the excess flow. This is discussed more fully in the following section.

## (E) Cherokee Wash Crossing

One of the issues driving this project is the limitation of access to Cherokee School during small storm events. Cherokee School is located on the east side of 56<sup>th</sup> Street between Cherokee Wash and Doubletree Ranch Road. The existing Cherokee Wash crossing consists of only a dip section. Therefore, there is water crossing the roadway during any runoff event. Doubletree Ranch Road becomes flooded as well during relatively small storms, thus isolating Cherokee School. Under the proposed plan, access will be possible from Doubletree Ranch Road during a 10-year storm event. Providing a 10-year crossing at Cherokee Wash will allow a second access to the school. A 4 barrel 10' X3' RCBC is proposed for the crossing. The northern-most barrel will discharge into the 56<sup>th</sup> Street lateral. The remaining three barrels will discharge into Cherokee Wash east of 52<sup>nd</sup> Street. A short concrete wall at the northern-most barrel will allow low flows to continue in Cherokee Wash during all storms which will help support the existing vegetative habitat downstream from 56<sup>th</sup> Street. A handrail along each face of the RCBC is preferred by the Town of Paradise Valley over guardrail or any other type of barrier.

The effect of adding a box culvert at this location is investigated. Under existing conditions, the channel upstream of 56<sup>th</sup> Street has less than a 10-year capacity, as substantiated by an FCDMC two-dimensional hydraulic model. Once channel capacity is exceeded, runoff will flow northeasterly towards Doubletree Ranch Road. About 200 feet upstream of 56<sup>th</sup> Street, the channel capacity is 300 cfs, which is less than half of the 10-year flow 789 cfs. The hydraulic effect of the culvert before and after improvements is determined for the 300 cfs flow rate, using a HEC-RAS model. As shown in a comparative stream profile plot in the **Appendix**, there would be no increase in water surface elevation after the culvert is constructed.

The culvert is designed for the full 10-year flow rate of 789 cfs. At some point in the future,

channel improvements may be made to Cherokee Wash to contain the 10-year flow. Of the 789 cfs, 184 cfs would be intercepted by the 56<sup>th</sup> Street storm drain, and 605 cfs would continue downstream. The capacity of Cherokee Wash for a short distance downstream of 56<sup>th</sup> Street is about 605 cfs. The Cherokee Wash cross section locations and HEC-RAS model output are presented in the **Appendix**. The diskette at the rear of the report contains the HEC-RAS input and output files.

# (F) Indian Bend Wash Outlet

The Doubletree Ranch Road storm drain daylights near Indian Bend Wash. At the storm drain outlet, riprap is placed for erosion protection. The storm drain exit velocity will be about 9.5 feet per second, and the 100-foot length of riprap should act to slow this down to the channel velocity of 4.2 feet per second. The riprap apron is set on the same grade as the grass lined swale, which is at a slope of 0.18 percent. The grass-lined swale conveys the flow to the low flow channel of the IBW. The **Appendix** contains the riprap protection design, and the grass-lined channel computations.

# APPENDIX B Cherokee Wash at 56<sup>th</sup> Street Culvert Calculations



# **Culvert Designer/Analyzer Report A1**

Analysis Co	omponent				
Storm Ever	nt E	Design [	Discharge		1,813.00 cfs
Peak Disch	arge Method: User-Spe	ecified			
Design Disc	charge 1,8	13.00 cfs (	Check Dischar	ge	1,813.00 cfs
Tailwater Co	onditions: Constant Tail	water			
Tailwater E	levation	N/A ft			
Name	Description	Discharge	HW Elev.	Velocity	
Culvert-1	3-10 x 3 ft Box	870.81 cfs	6.51 ft	9.77 ft/s	-
Culvert-2	1-60 inch Circular	149.81 cfs	6.51 ft	10.18 ft/s	
Weir	Roadway	792.69 cfs	6.51 ft	N/A	
Total		1,813.32 cfs	6.51 ft	N/A	_

# **Culvert Designer/Analyzer Report**

# Component:Culvert-1

Culvert Summary					
Computed Headwater Eleva	6.51	ft	Discharge	870.81	cfs
Inlet Control HW Elev.	6.29	ft	Tailwater Elevation	N/A	ft
Outlet Control HW Elev.	6.51	ft	Control Type	Outlet Control	
Headwater Depth/Height	1.84				
Grades					
Upstream Invert	1.00	ft	Downstream Invert	0.83	ft
Length	85.00	ft	Constructed Slope	0.002000	ft/ft
Hydraulic Profile					
Profile CompositeM2Pres	ssureProfile		Depth, Downstream	2.97	ft
Slope Type	Mild		Normal Depth	N/A	ft
Flow Regime	Subcritical		Critical Depth	2.97	ft
Velocity Downstream	9.77	ft/s	Critical Slope	0.003190	ft/ft
Section					
Section Shape	Box		Mannings Coefficient	0.013	
Section Material	Concrete		Span	10.00	ft
Section Size	10 x 3 ft		Rise	3.00	
Number Sections	3				
Outlet Control Properties					
Outlet Control HW Elev.	6.51	ft	Upstream Velocity Head	1.45	ft
Ke	0.50		Entrance Loss	0.73	ft
Inlet Control Properties					
Inlet Control HW Elev.	6.29	ft	Flow Control	Submerged	
Inlet Type 45° wingwall flare			Area Full	90.0	ft²
K	0.51000		HDS 5 Chart	9	
M	0.66700		HDS 5 Scale	1	
С	0.03090		Equation Form	2	
Υ	0.80000		•		

# Culvert Designer/Analyzer Report A1

# Component:Culvert-2

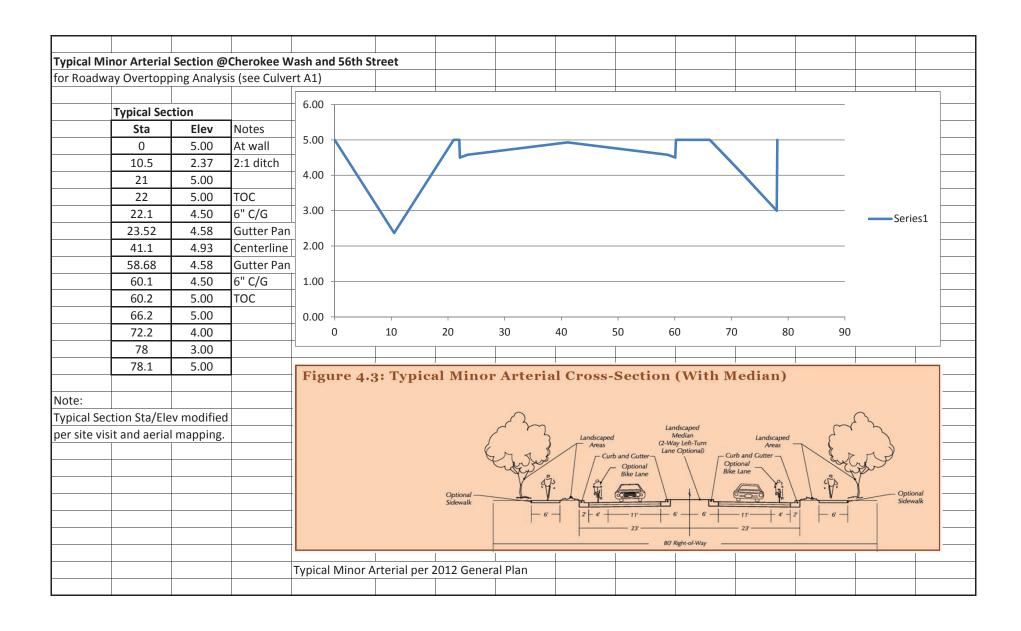
Culvert Summary					
Computed Headwater Eleva	6.51	ft	Discharge	149.81	cfs
Inlet Control HW Elev.	6.31	ft	Tailwater Elevation	N/A	ft
Outlet Control HW Elev.	6.51	ft	Control Type	Outlet Control	
Headwater Depth/Height	1.10				
Grades					
Upstream Invert	1.00	ft	Downstream Invert	0.85	ft
Length	85.00	ft	Constructed Slope	0.001800	ft/ft
Hydraulic Profile					
Profile	M2		Depth, Downstream	3.51	ft
Slope Type	Mild		Normal Depth	N/A	ft
Flow Regime	Subcritical		Critical Depth	3.51	ft
Velocity Downstream	10.18	ft/s	Critical Slope	0.004689	ft/ft
Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Section Material	Concrete		Span	5.00	ft
Section Size	60 inch		Rise	5.00	
Number Sections	1				
Outlet Control Properties					
Outlet Control HW Elev.	6.51	ft	Upstream Velocity Head	1.17	ft
Ke	0.20		Entrance Loss	0.23	ft
Inlet Control Properties					
Inlet Control HW Elev.	6.31	ft	Flow Control	Unsubmerged	
Inlet Type Beveled ring, 3	3.7° bevels		Area Full	19.6	ft²
K	0.00180		HDS 5 Chart	3	
M	2.50000		HDS 5 Scale	В	
С	0.02430		Equation Form	1	
Υ	0.83000				

# **Culvert Designer/Analyzer Report**

# Component:Weir

Hydraulic Component(s): Ro	adway		
Discharge	792.69 cfs	Allowable HW Elevation	6.51 ft
Roadway Width	38.00 ft	Overtopping Coefficient	3.02 US
Low Point	2.37 ft	Headwater Elevation	6.51 ft
Discharge Coefficient (Cr)	3.02	Submergence Factor (Kt)	1.00
Tailwater Elevation	-9,999.00 ft		

Sta (ft)	Elev. (ft)
0.00	5.00
10.50	2.37
21.00	5.00
22.00	5.00
22.10	4.50
23.52	4.58
41.10	4.93
56.68	4.58
60.10	4.50
60.20	5.00
66.20	5.00
72.20	4.00
78.00	2.75
80.00	5.00



# APPENDIX C Flowsplit Calculations East of 56<sup>th</sup> Street



# E Caballo Drive(A2)

# **Project Description**

Friction Method Manning Formula Solve For Discharge

# Input Data

 $\begin{array}{ccc} \text{Channel Slope} & 0.00260 & \text{ft/ft} \\ \text{Normal Depth} & 1.10 & \text{ft} \end{array}$ 

Section Definitions

Station (ft)		Elevation (ft)	
	0+00		5.80
	0+08		4.80
	0+10		4.30
	0+28		4.66
	0+46		4.30
	0+48		4.80
	0+63		5.40

### Roughness Segment Definitions

Start Station		Ending Station		Roughness Coefficient	
	(0+00, 5.80)		(0+63, 5.40)		0.016

# **Options**

Current Roughness Weighted Method
Open Channel Weighting Method
Pavlovskii's Method
Closed Channel Weighting Method
Pavlovskii's Method

### Results

Discharge		159.71	ft³/s
Elevation Range	4.30 to 5.80 ft		
Flow Area		42.46	ft²
Wetted Perimeter		59.98	ft
Hydraulic Radius		0.71	ft
Top Width		59.80	ft

# E Caballo Drive(A2)

	E dabane Brive(/ (2)
Results	
Normal Depth	1.10 ft
Critical Depth	0.98 ft
Critical Slope	0.00436 ft/ft
Velocity	3.76 ft/s
Velocity Head	0.22 ft
Specific Energy	1.32 ft
Froude Number	0.79
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	1.10 ft
Critical Depth	0.98 ft
Channel Slope	0.00260 ft/ft
Critical Slope	0.00436 ft/ft

	o Drive)	_						
Sta	Elev							
0	5.8							
8	4.8	Edge of S/W						
10	4.3							
28	4.66	Centerline						
46	4.3							
48	4.8	Edge of S/W						
63	5.4							
Notes:								
Section based of	n measuremen	t in Google Earth	1					
and PV typical r								
		nt between walls	s.					
Address or	rintersection	Q	THE STATE OF THE S		MEMORISAN TO A SECOND	COLUMN TO SERVICE	33944 C389	
188'					A			
188° 0"E 225'		antella Dr		63.1'	12PTY-B-0-6/AH			

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# **Project Description**

Friction Method Manning Formula
Solve For Discharge

# Input Data

 Channel Slope
 0.00500
 ft/ft

 Normal Depth
 1.69
 ft

Section Definitions

Station (ft)	Elevation (ft)
otation (it)	Lievanon (n)
0+00	1341.33
0+06	1341.14
0+11	1340.93
0+14	1339.30
0+15	1338.97
0+16	1338.96
0+29	1338.86
0+35	1338.81
0+44	1339.56
0+63	1340.67

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient	
(0+00, 1341.33)	(0+63, 1340.67)		0.030

# **Options**

Current Roughness Weighted Pavlovskii's Method
Open Channel Weighting Method Pavlovskii's Method
Closed Channel Weighting Method Pavlovskii's Method

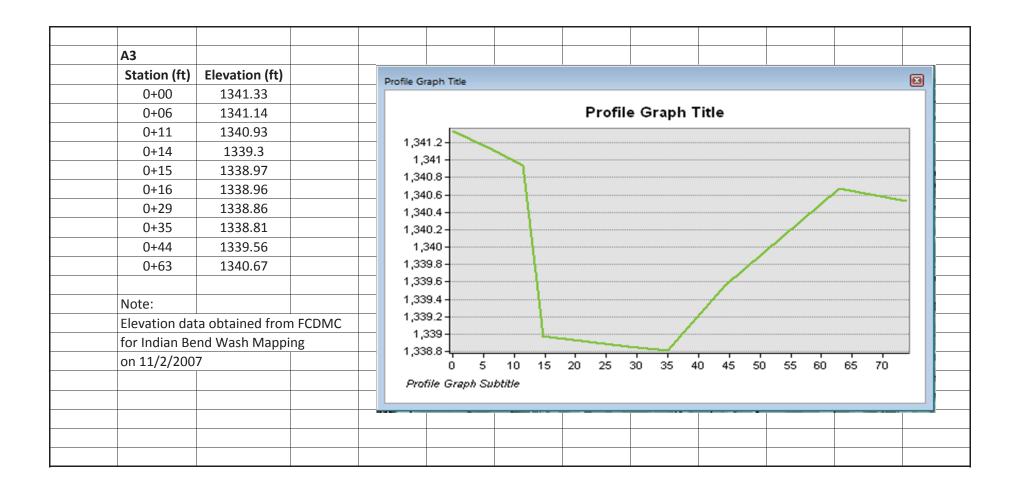
### Results

 Discharge
 205.28
 ft³/s

 Elevation Range
 1338.81 to 1341.33 ft

 Flow Area
 54.30
 ft²

		A3		
Results				
Wetted Perimeter		48.41	ft	
Hydraulic Radius		1.12	ft	
Top Width		47.93	ft	
Normal Depth		1.69	ft	
Critical Depth		1.32	ft	
Critical Slope		0.01365	ft/ft	
Velocity		3.78	ft/s	
Velocity Head		0.22	ft	
Specific Energy		1.91	ft	
Froude Number		0.63		
Flow Type	Subcritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	ft/s	
Normal Depth		1.69	ft	
Critical Depth		1.32	ft	
Channel Slope		0.00500	ft/ft	
Critical Slope		0.01365	ft/ft	



# A4

# **Project Description**

Friction Method Manning Formula
Solve For Discharge

# Input Data

Section Definitions

Station (ft)     Elevation (ft)       0+93     1333.66       0+94     1333.50       0+97     1333.35       1+01     1333.08       1+04     1332.96       1+12     1334.34       1+13     1334.67			
0+94       1333.50         0+97       1333.35         1+01       1333.08         1+04       1332.96         1+12       1334.34	Station (ft)		Elevation (ft)
0+94       1333.50         0+97       1333.35         1+01       1333.08         1+04       1332.96         1+12       1334.34			
0+97       1333.35         1+01       1333.08         1+04       1332.96         1+12       1334.34		0+93	1333.66
1+01     1333.08       1+04     1332.96       1+12     1334.34		0+94	1333.50
1+04 1332.96 1+12 1334.34		0+97	1333.35
1+12 1334.34		1+01	1333.08
		1+04	1332.96
1+13 1334.67		1+12	1334.34
		1+13	1334.67

Roughness Segment Definitions

S	start Station	Ending Station	Roughness Coefficient
	(0+93, 1333.66)	(1+13, 1334.6)	7) 0.030

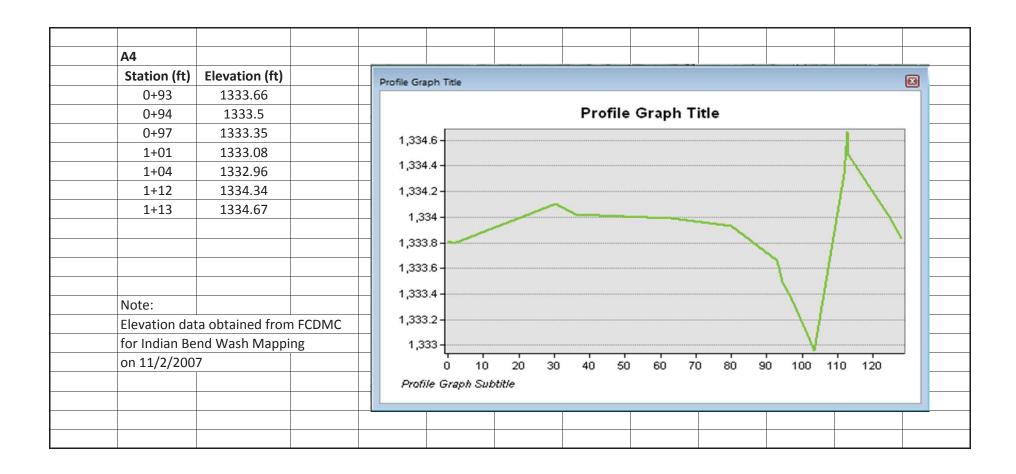
# **Options**

Current Roughness Weighted Method Pavlovskii's Method Open Channel Weighting Method Pavlovskii's Method Closed Channel Weighting Method Pavlovskii's Method

### Results

Discharge	6.87	ft³/s
Elevation Range	1332.96 to 1334.67 ft	
Flow Area	5.51	ft²
Wetted Perimeter	14.96	ft
Hydraulic Radius	0.37	ft
Top Width	14.88	ft

		A4		
Results				
Normal Depth		0.70	ft	
Critical Depth		0.47	ft	
Critical Slope		0.02142	ft/ft	
Velocity		1.25	ft/s	
Velocity Head		0.02	ft	
Specific Energy		0.72	ft	
Froude Number		0.36		
Flow Type	Subcritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	ft/s	
Normal Depth		0.70	ft	
Critical Depth		0.47	ft	
Channel Slope		0.00240	ft/ft	
Critical Slope		0.02142	ft/ft	



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# **Project Description**

Friction Method Manning Formula
Solve For Discharge

# Input Data

 $\begin{array}{ccc} \text{Channel Slope} & 0.01500 & \text{ft/ft} \\ \text{Normal Depth} & 0.89 & \text{ft} \end{array}$ 

Section Definitions

Station (ft)		Elevation (ft)
C	0+00	1335.78
C	0+13	1335.74
C	0+24	1335.68
C	0+26	1335.66
C	0+37	1335.60
C	0+47	1335.53
C	0+53	1335.18
C	0+61	1335.13
C	0+74	1335.04
C	0+80	1334.40
C	0+80	1334.40
C	0+80	1334.40
C	0+87	1334.85
C	0+92	1335.34
C	0+98	1335.31
1	1+02	1335.29
1	1+09	1335.29

# Roughness Segment Definitions

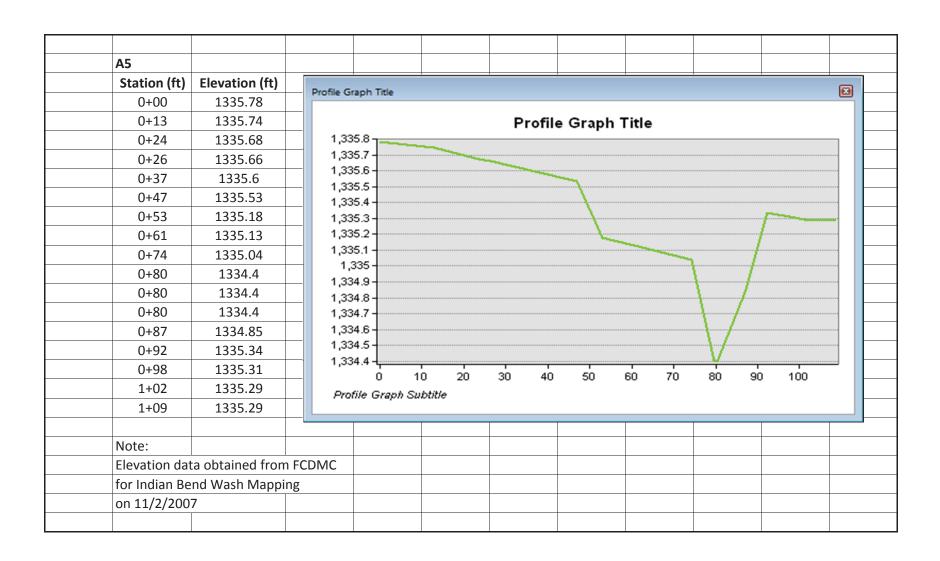
Start Station	Ending Station	Roughness Coefficient
(0+00, 1335.78)	(1+09, 1335.29)	0.030

# Options

Gurrent Roughness Weighted Pavlovskii's Method

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Options							
Open Channel Weighting Method	Pavlovskii's Method						
Closed Channel Weighting Method	Pavlovskii's Method						
Results							
Discharge		37.76	ft³/s				
Elevation Range	1334.40 to 1335.78 ft						
Flow Area		13.19	ft <sup>2</sup>				
Wetted Perimeter		40.66	ft				
Hydraulic Radius		0.32	ft				
Top Width		40.58	ft				
Normal Depth		0.89	ft				
Critical Depth		0.86	ft				
Critical Slope		0.01957	ft/ft				
Velocity		2.86	ft/s				
Velocity Head		0.13	ft				
Specific Energy		1.02	ft				
Froude Number		0.89					
Flow Type	Subcritical						
GVF Input Data							
Downstream Depth		0.00	ft				
Length		0.00	ft				
Number Of Steps		0					
GVF Output Data							
Upstream Depth		0.00	ft				
Profile Description							
Profile Headloss		0.00	ft				
Downstream Velocity		Infinity	ft/s				
Upstream Velocity		Infinity	ft/s				
Normal Depth		0.89	ft				
Critical Depth		0.86	ft				
Channel Slope		0.01500	ft/ft				
Critical Slope		0.01957	ft/ft				



Α6
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# **Project Description**

Friction Method Manning Formula
Solve For Discharge

# Input Data

 $\begin{array}{c} \text{Channel Slope} & 0.00350 & \text{ft/ft} \\ \text{Normal Depth} & 1.02 & \text{ft} \end{array}$ 

Section Definitions

Station (ft)	Elevation (ft)
0+16	1345.08
0+17	1345.08
0+24	1344.90
0+27	1344.46
0+29	1344.18
0+31	1343.96
0+36	1343.44
0+54	1343.42
0+65	1343.42
0+65	1343.77
0+67	1343.79
0+80	1343.51
0+85	1343.12
0+87	1342.92
0+89	1342.92
0+96	1342.95
1+14	1343.67
1+15	1343.69
1+16	1343.70
1+43	1343.94

Roughness Segment Definitions

Start Station		Ending Station		Roughness Coefficient	
(0-	+16, 1345.08)	(1	+43, 1343.94)		0.030

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Current Roughness Weighted Pavlovskii's Method Method Open Channel Weighting Method Pavlovskii's Method Closed Channel Weighting Method Pavlovskii's Method

#### Results

Discharge		84.06	ft³/s
Elevation Range	1342.92 to 1345.08 ft		
Flow Area		49.50	ft²
Wetted Perimeter		112.19	ft
Hydraulic Radius		0.44	ft
Top Width		112.00	ft
Normal Depth		1.02	ft
Critical Depth		0.77	ft
Critical Slope		0.01882	ft/ft
Velocity		1.70	ft/s
Velocity Head		0.04	ft
Specific Energy		1.07	ft
Froude Number		0.45	
Flow Type	Subcritical		

#### **GVF Input Data**

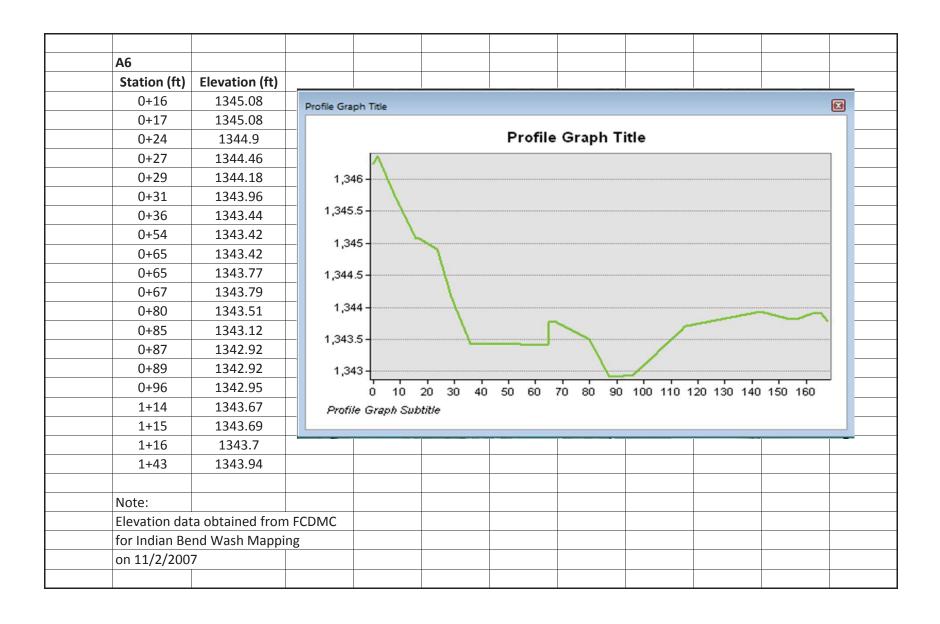
0.00 ft Downstream Depth 0.00 Length Number Of Steps 0

#### **GVF Output Data**

Upstream Depth

Profile Description Profile Headloss 0.00 ft Downstream Velocity Infinity ft/s Infinity Upstream Velocity ft/s 1.02 Normal Depth ft Critical Depth 0.77 ft Channel Slope 0.00350 ft/ft Critical Slope 0.01882 ft/ft

0.00 ft

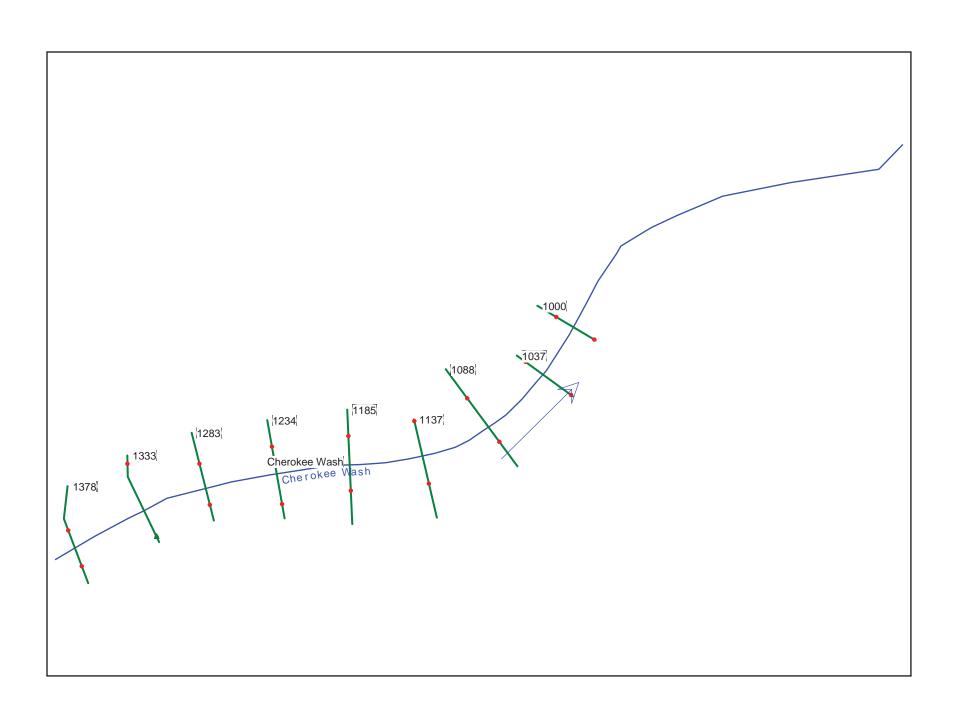


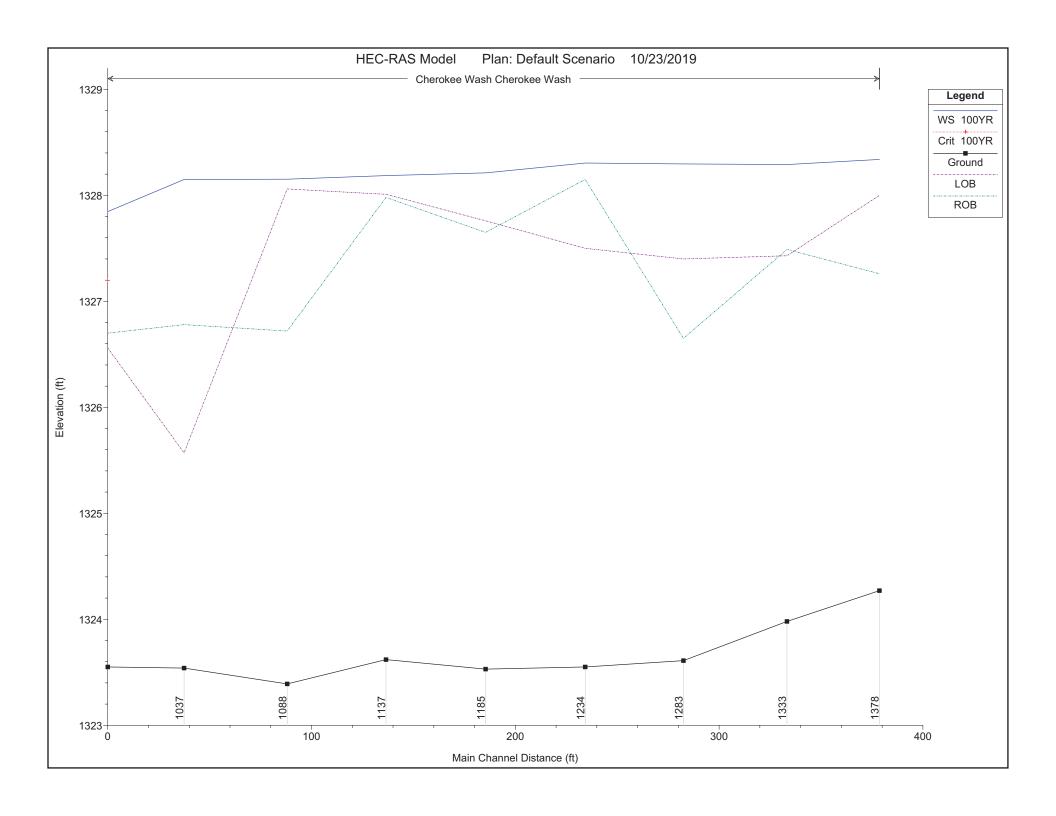
# APPENDIX D HEC-RAS Analysis for Cherokee Wash at the Site

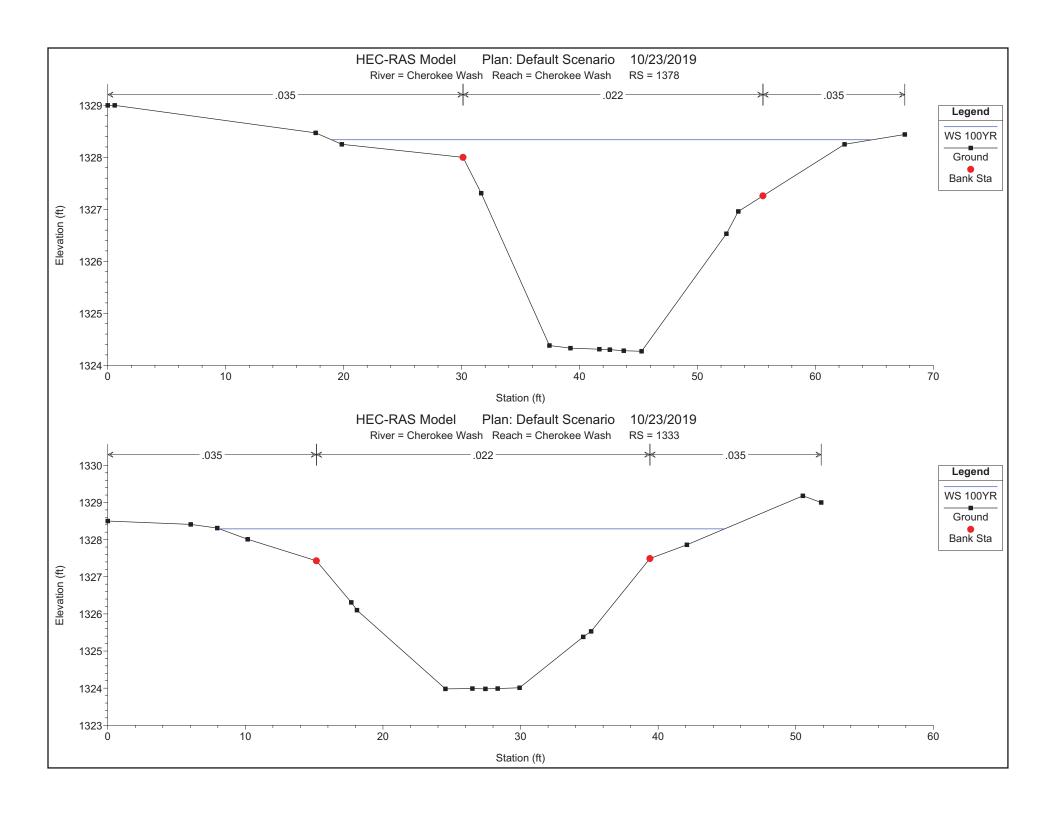


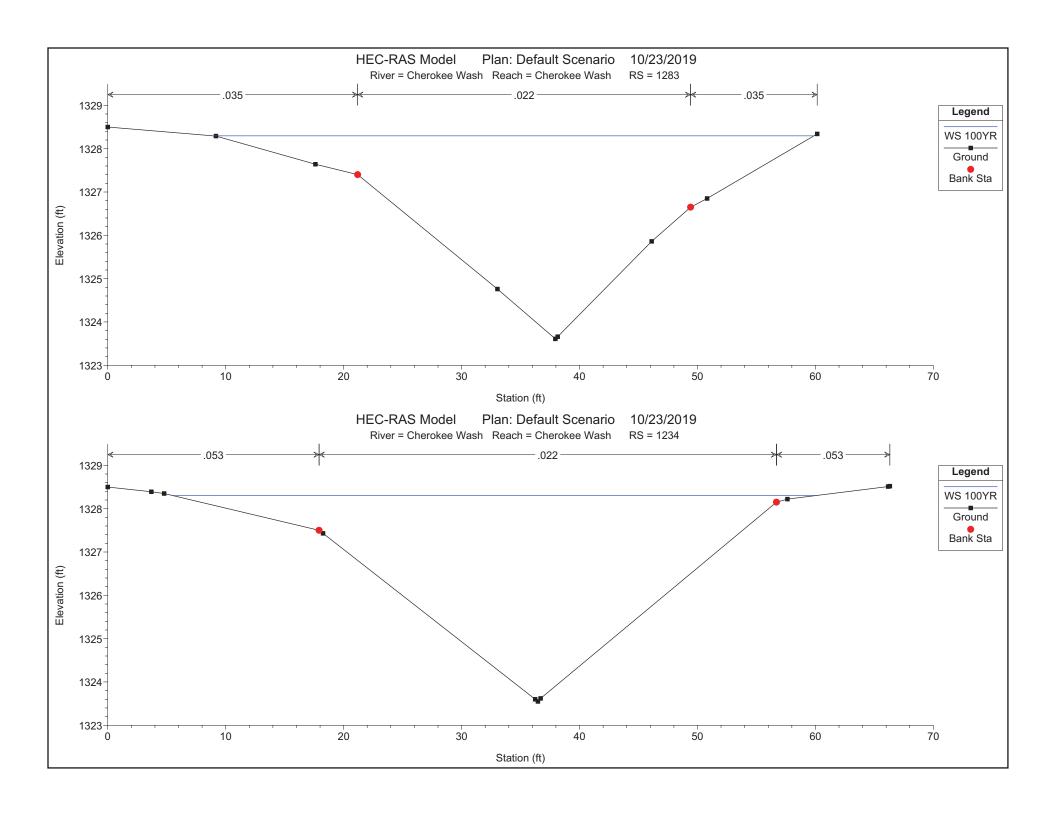
## **Existing Condition**

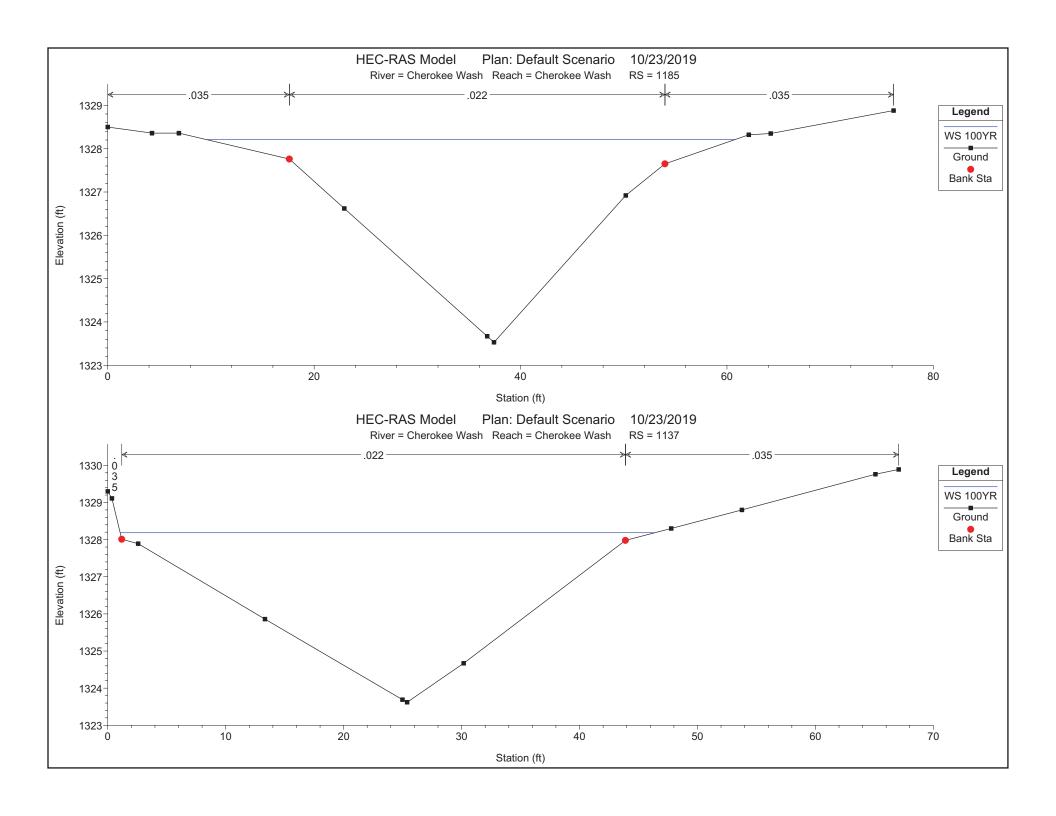


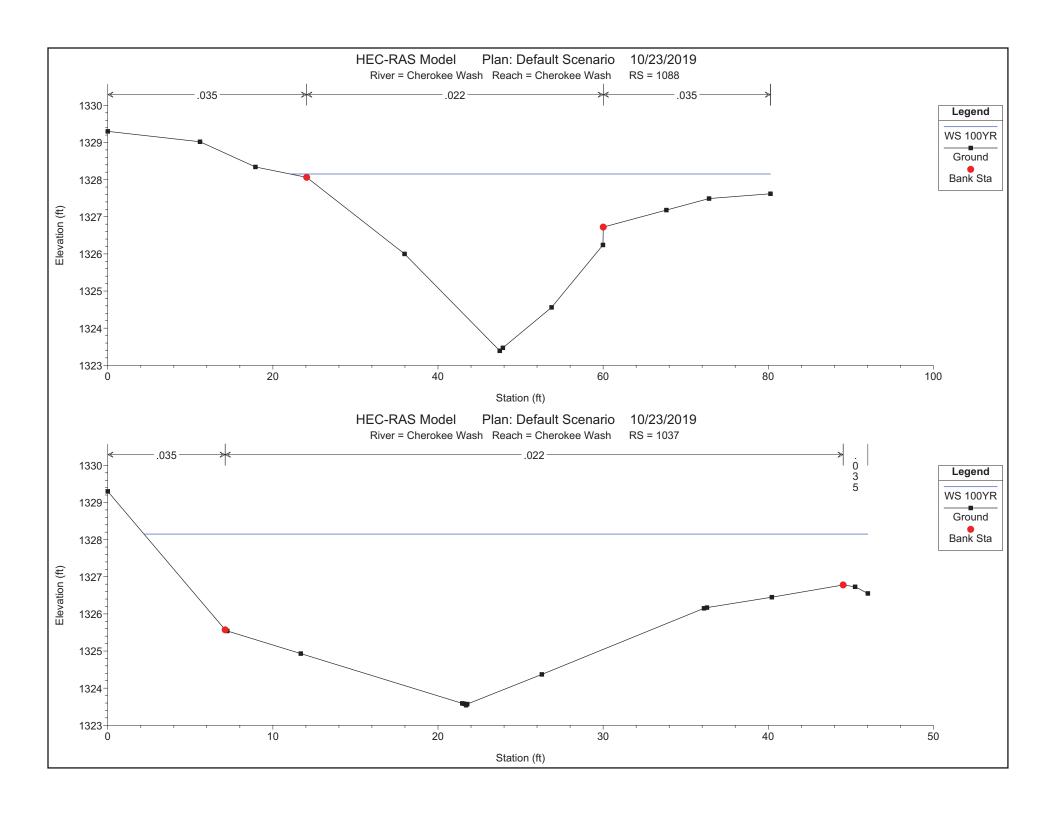


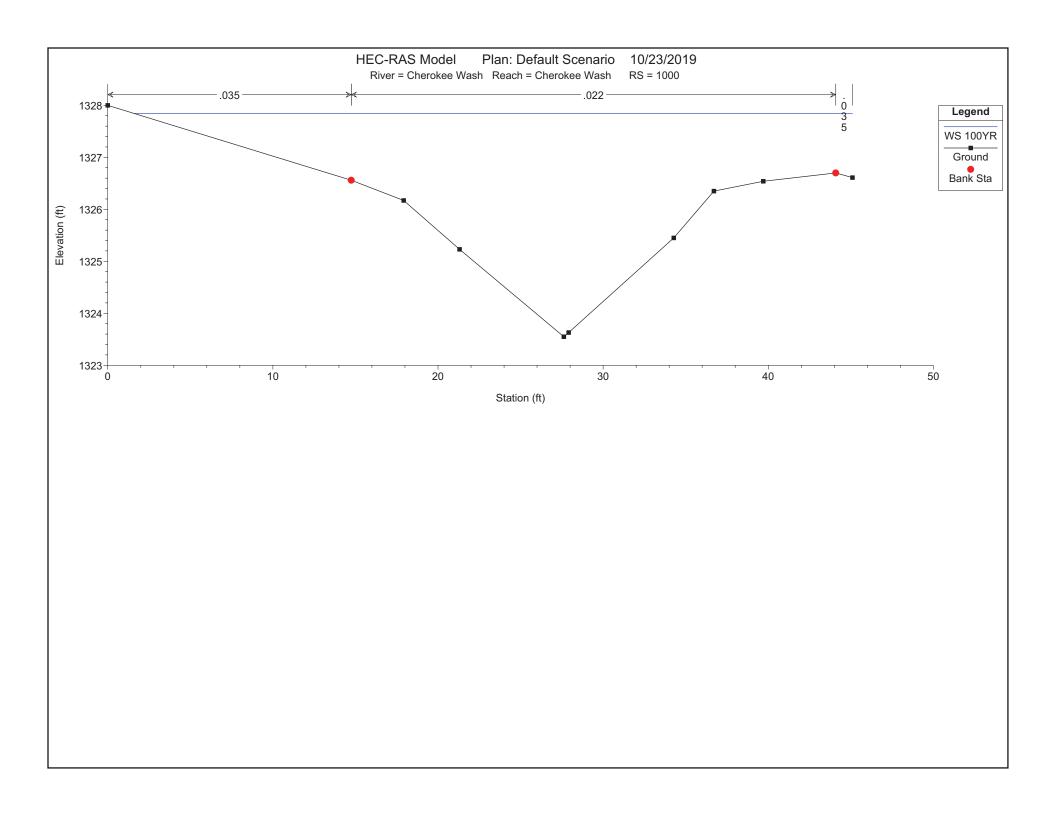










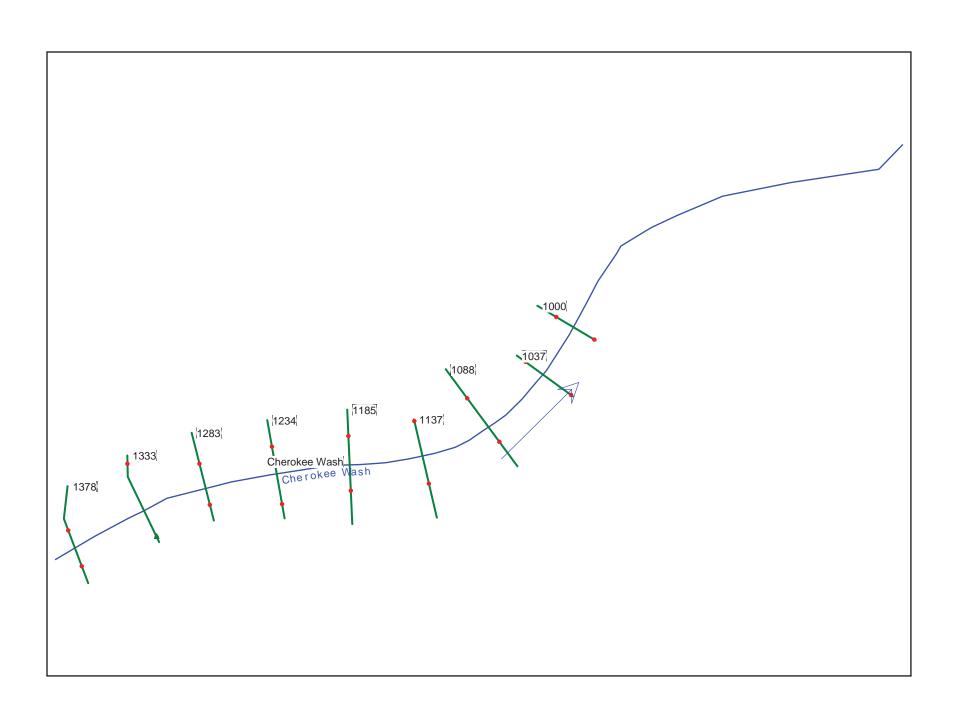


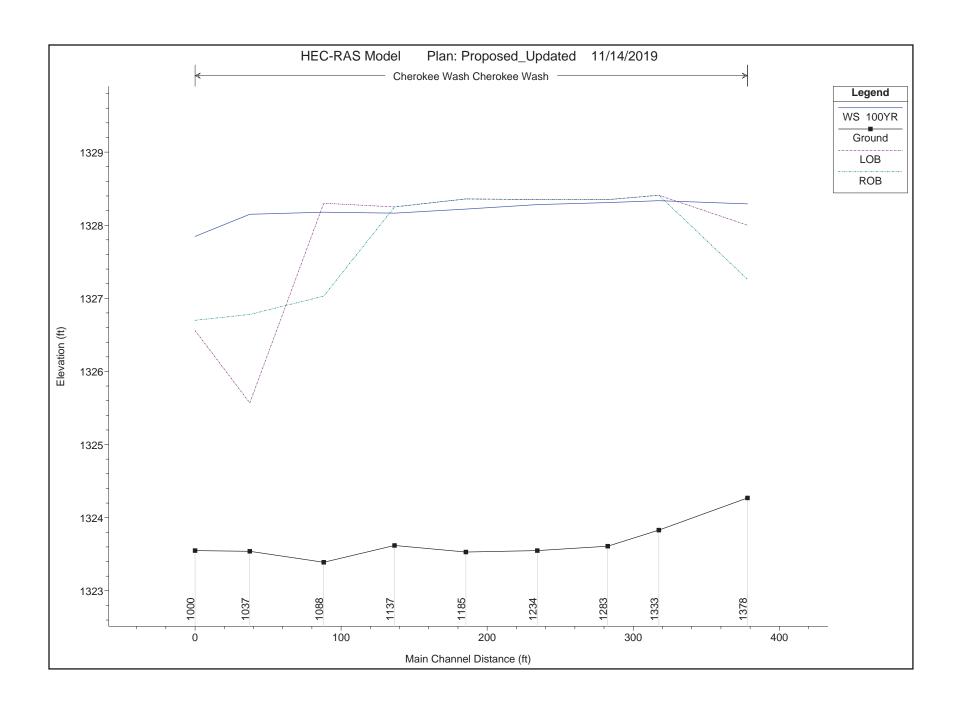
HEC-RAS Plan: Default Scenario River: Cherokee Wash Reach: Cherokee Wash Profile: 100YR

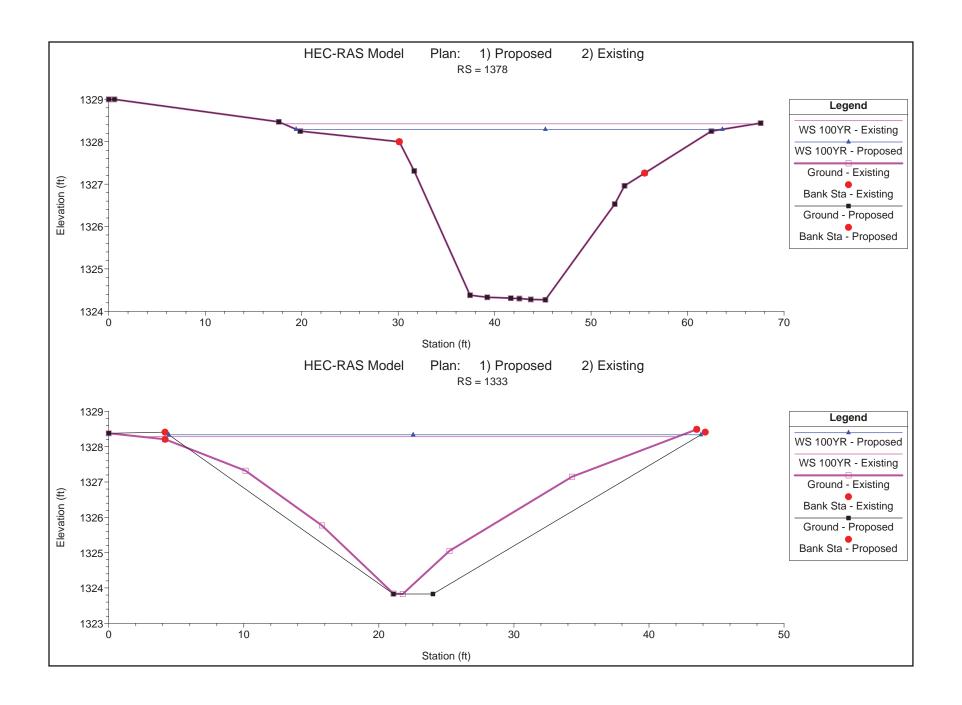
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Cherokee Wash	1378	100YR	378.00	1324.27	1328.34		1328.75	0.001550	5.16	78.62	45.90	0.54
Cherokee Wash	1333	100YR	378.00	1323.98	1328.29		1328.68	0.001324	5.02	79.78	36.73	0.50
Cherokee Wash	1283	100YR	378.00	1323.61	1328.30		1328.59	0.001062	4.41	96.62	51.01	0.45
Cherokee Wash	1234	100YR	378.00	1323.55	1328.30		1328.52	0.000873	3.72	106.24	54.63	0.41
Cherokee Wash	1185	100YR	378.00	1323.53	1328.21		1328.47	0.001077	4.06	96.34	51.28	0.45
Cherokee Wash	1137	100YR	378.00	1323.62	1328.19		1328.40	0.001006	3.75	101.14	45.33	0.43
Cherokee Wash	1088	100YR	378.00	1323.39	1328.15		1328.36	0.000845	3.71	114.48	58.21	0.40
Cherokee Wash	1037	100YR	378.00	1323.54	1328.15		1328.31	0.000526	3.24	122.71	43.84	0.33
Cherokee Wash	1000	100YR	378.00	1323.55	1327.85	1327.20	1328.25	0.001902	5.18	80.07	43.53	0.59

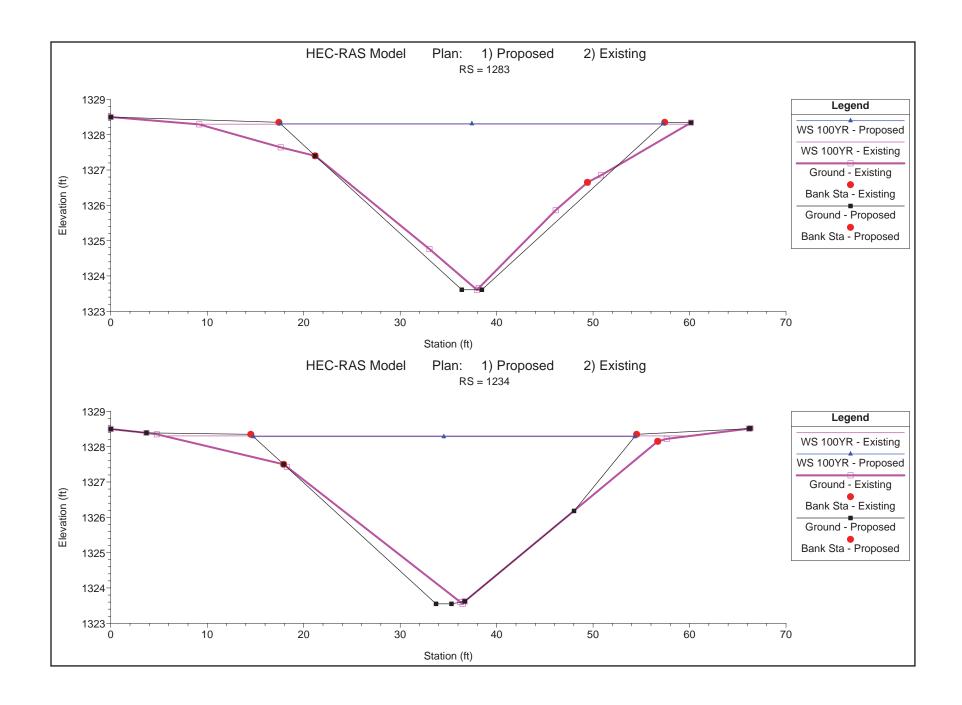
## **Proposed Condition**

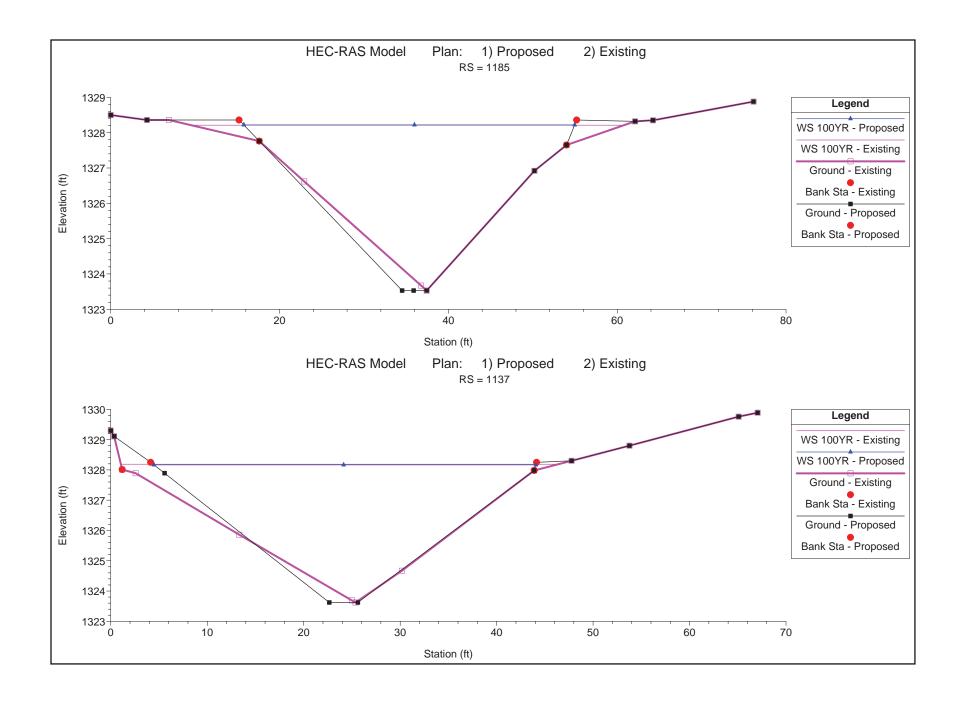


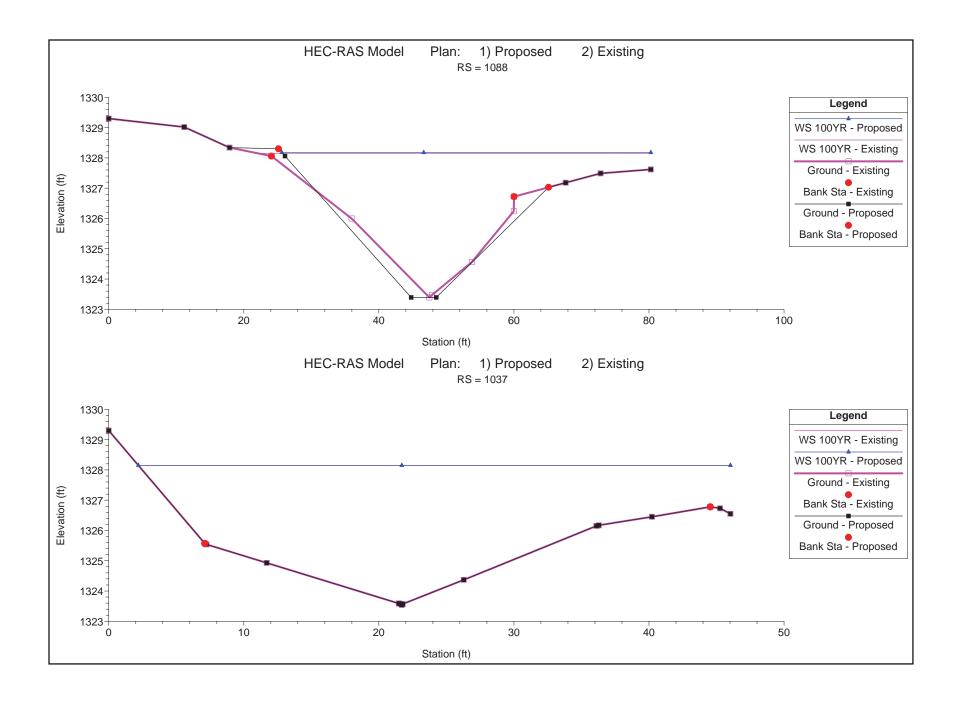


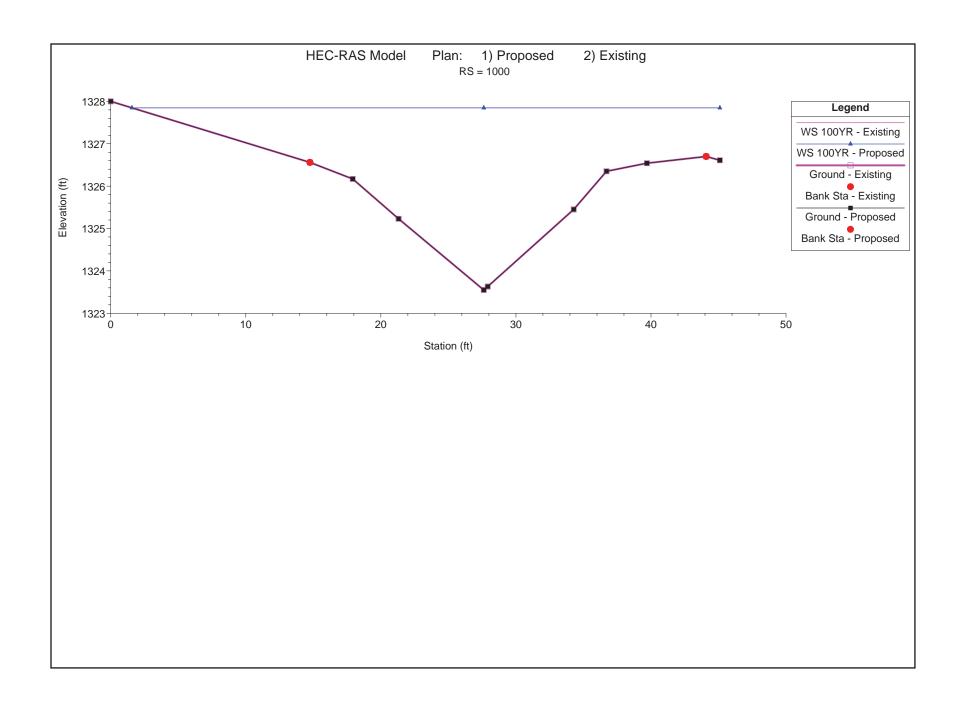












HEC-RAS Plan: Proposed River: Cherokee Wash Reach: Cherokee Wash Profile: 100YR

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Cherokee Wash	1378	100YR	378.00	1324.27	1328.29		1328.72	0.001643	5.25	76.52	44.18	0.55
Cherokee Wash	1333	100YR	378.00	1323.83	1328.34	1327.01	1328.58	0.001100	3.96	95.34	41.34	0.45
Cherokee Wash	1283	100YR	378.00	1323.61	1328.31		1328.54	0.001008	3.85	98.20	39.68	0.43
Cherokee Wash	1234	100YR	378.00	1323.55	1328.28		1328.49	0.000837	3.64	103.73	39.52	0.40
Cherokee Wash	1185	100YR	378.00	1323.53	1328.22		1328.44	0.000946	3.79	99.70	39.20	0.42
Cherokee Wash	1137	100YR	378.00	1323.62	1328.17		1328.40	0.001012	3.86	98.00	39.58	0.43
Cherokee Wash	1088	100YR	378.00	1323.39	1328.18		1328.34	0.000591	3.26	124.72	54.64	0.34
Cherokee Wash	1037	100YR	378.00	1323.54	1328.15		1328.31	0.000526	3.24	122.73	43.84	0.33
Cherokee Wash	1000	100YR	378.00	1323.55	1327.85	1327.20	1328.25	0.001901	5.18	80.08	43.53	0.59

## PLATE 1 Drainage Map



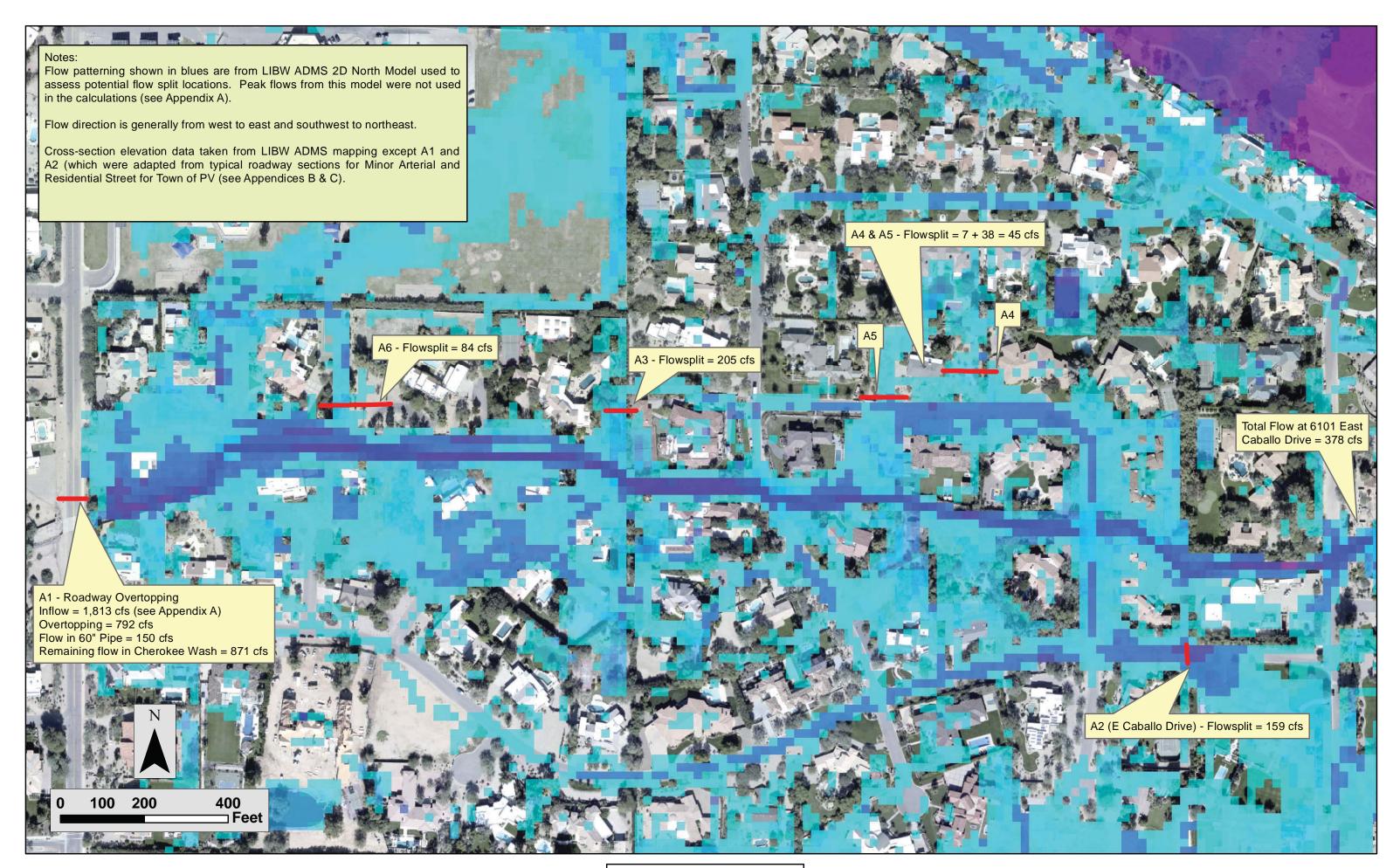
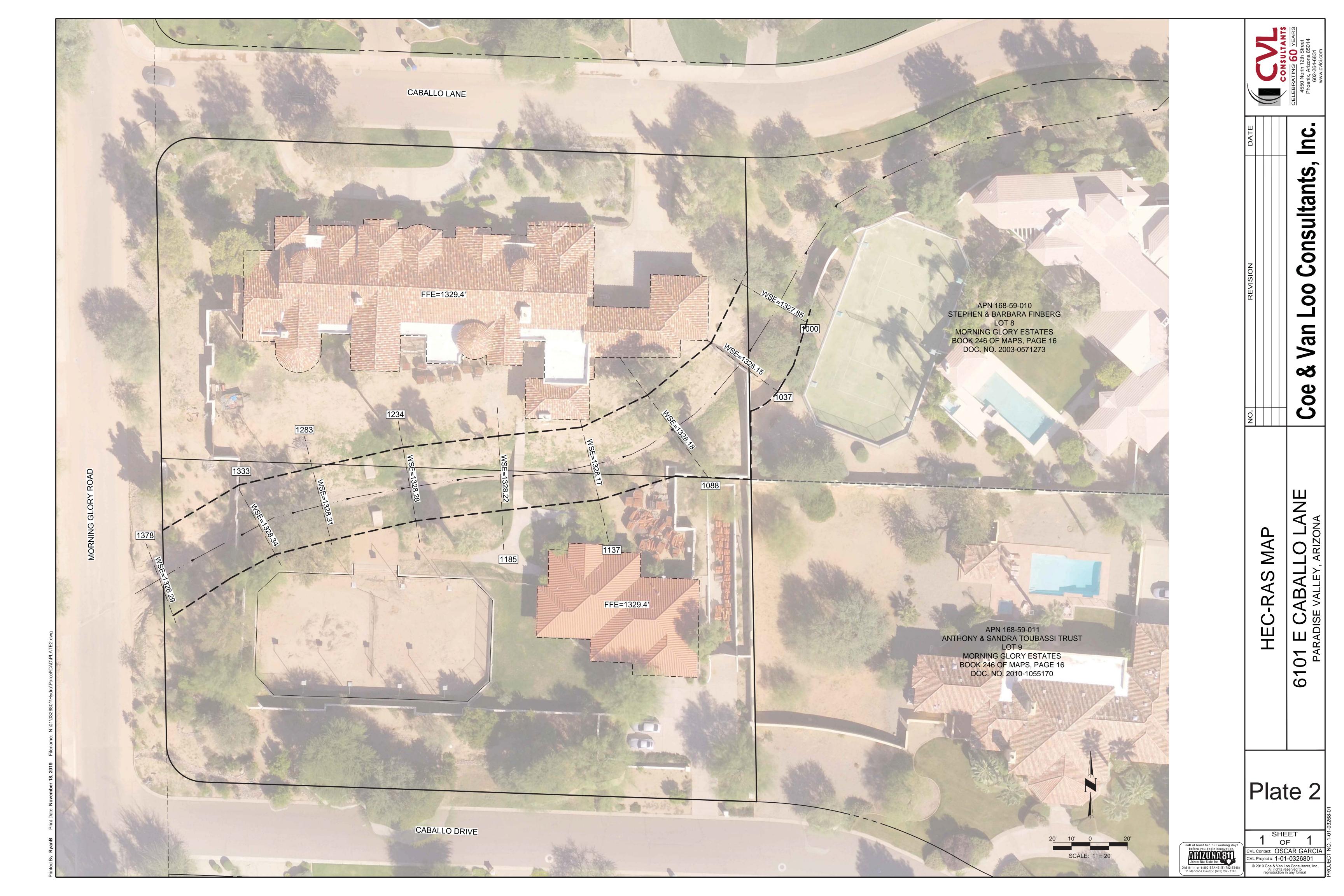


Plate 1 - Drainage Map

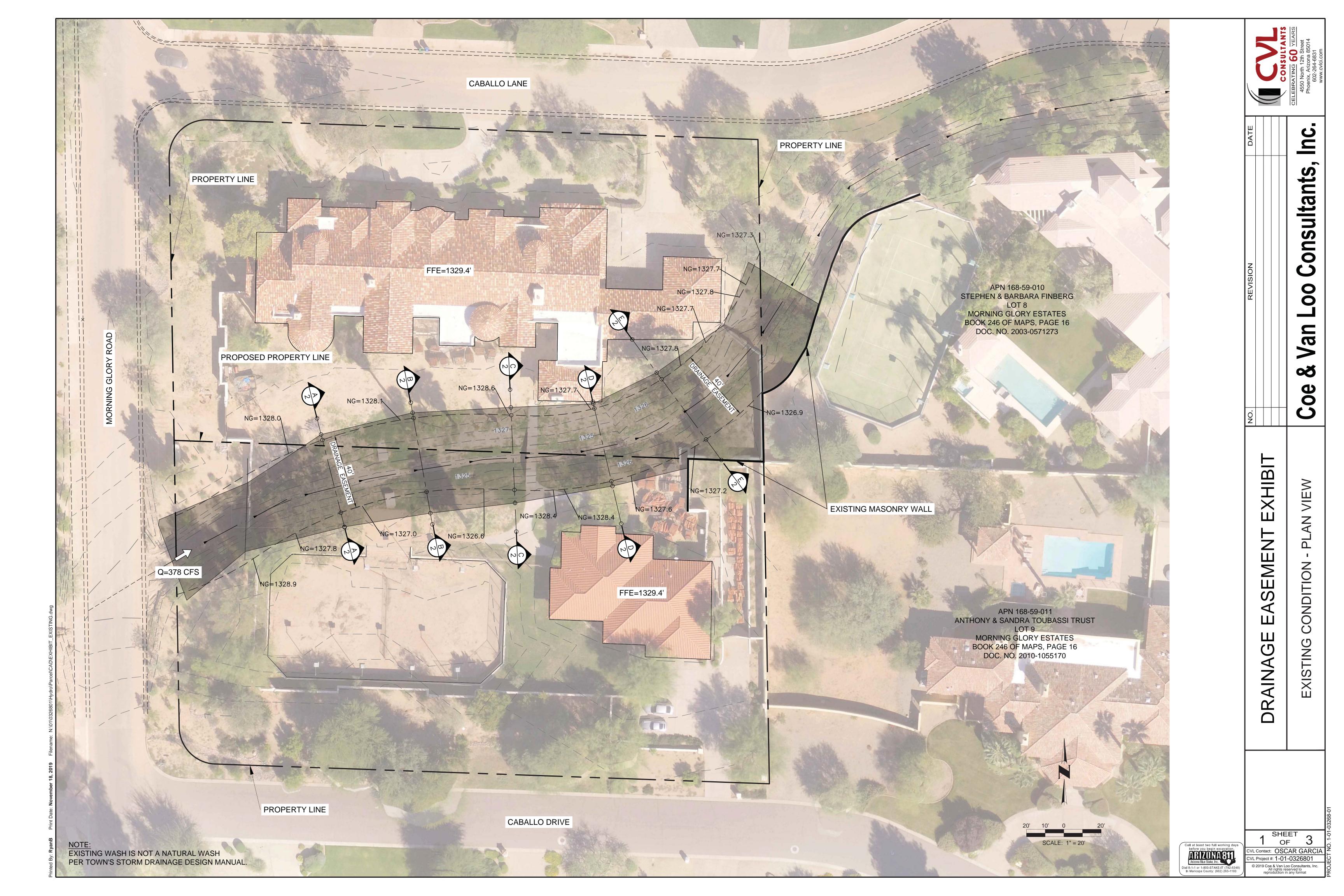
## PLATE 2 HEC-RAS Map

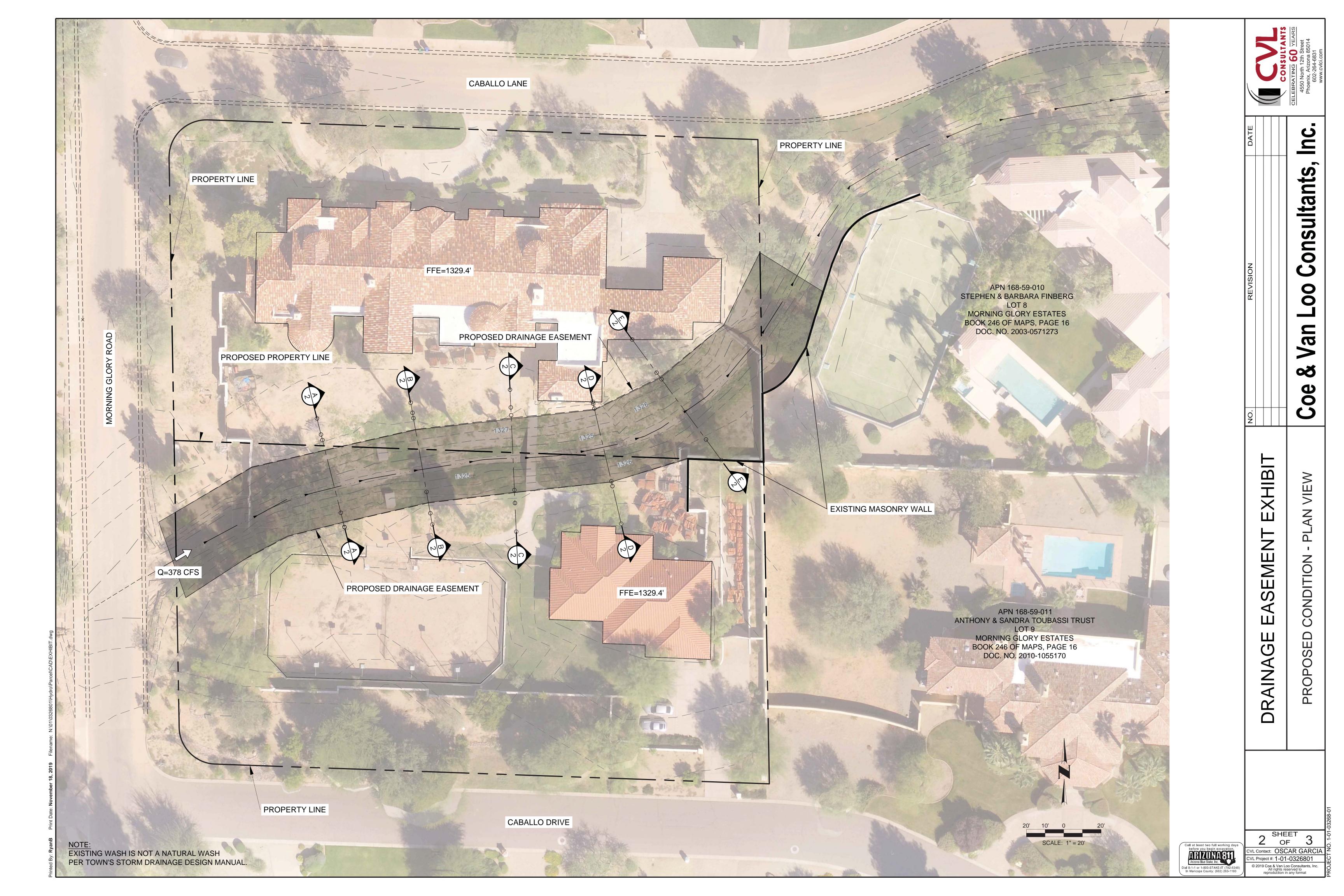


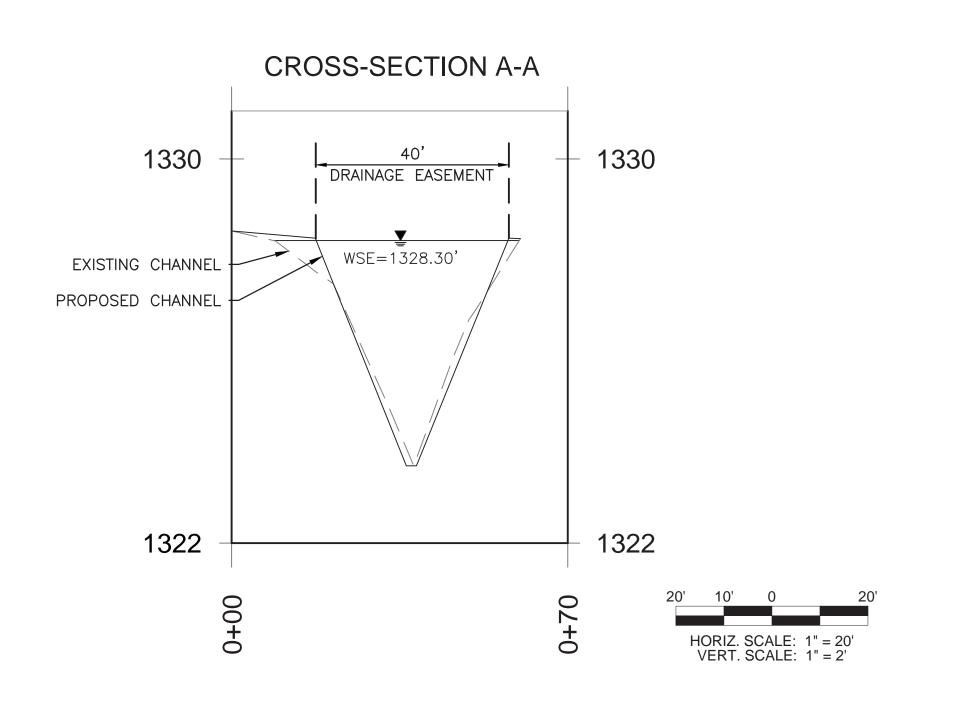


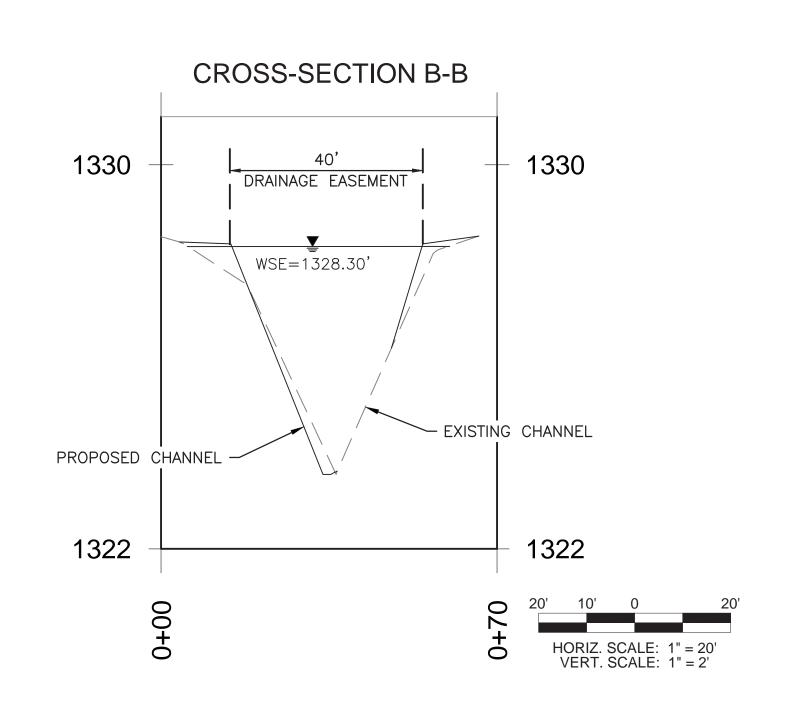
### **DRAINAGE EASEMENT EXHIBIT**

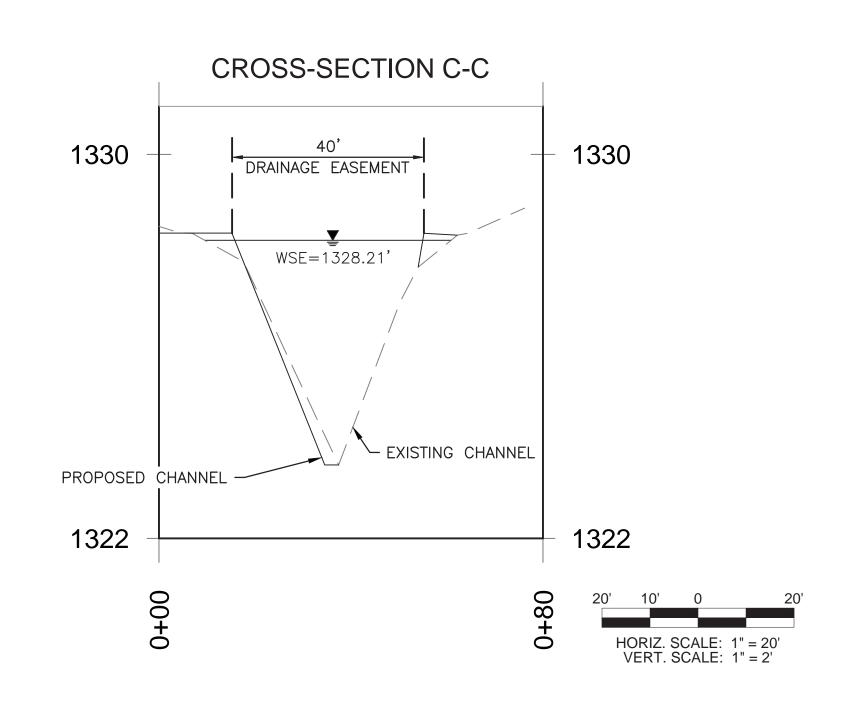


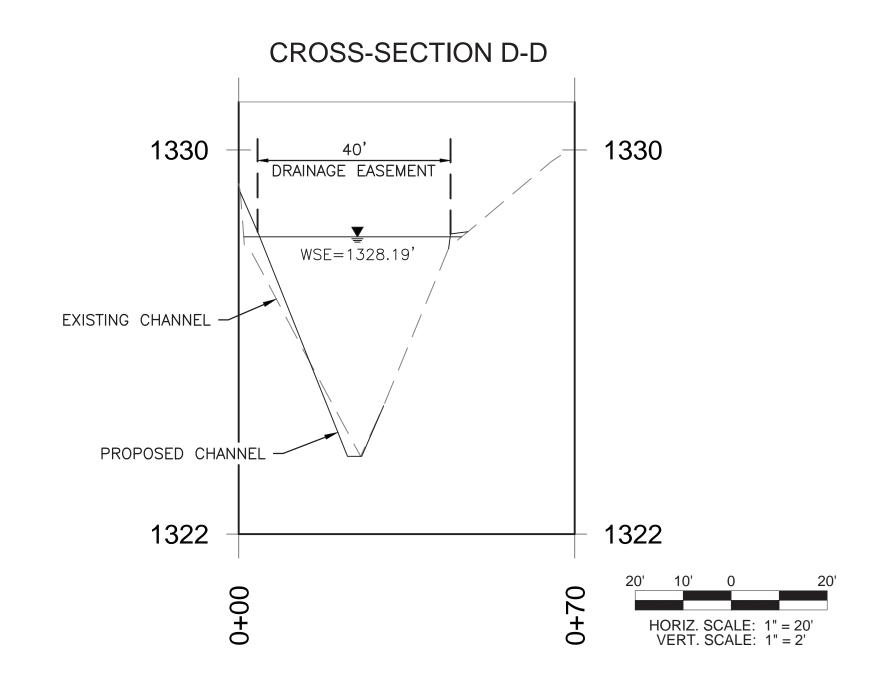


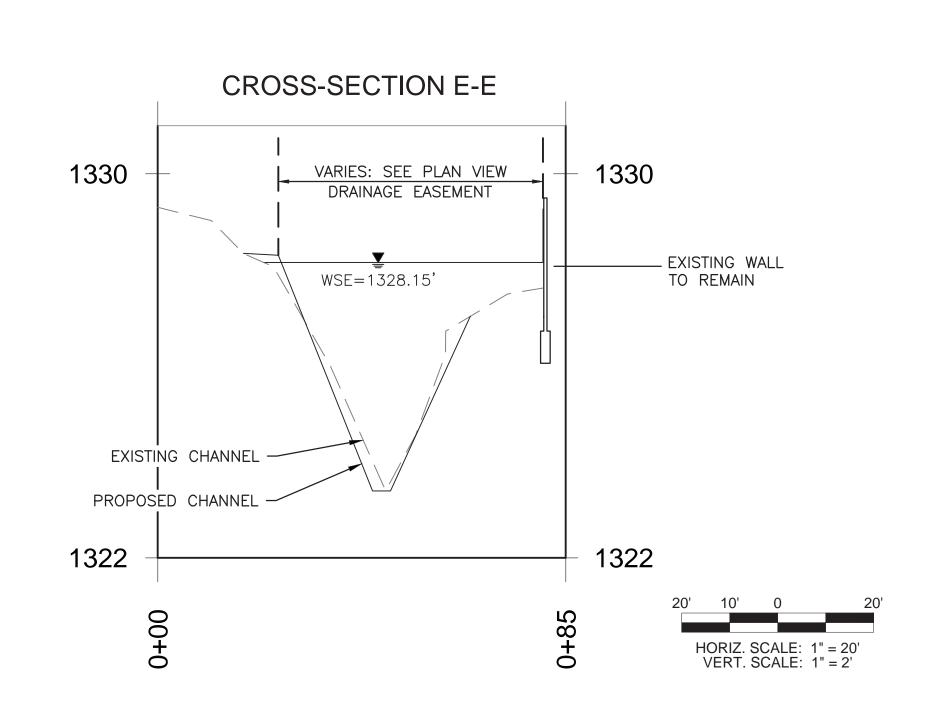


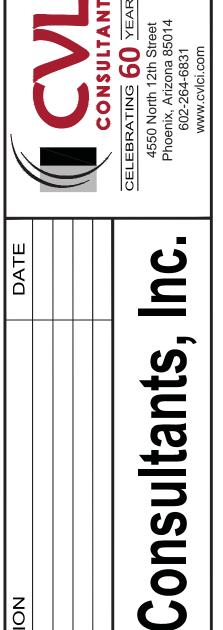












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