ROCK CUT SLOPE STABILITY ANALYSIS

PROPOSED CUSTOM HILLSIDE RESIDENCE APN 169-04-007 7550 NORTH HUMMINGBIRD LANE PARADISE VALLEY, ARIZONA 85253

Prepared for:

Mr. Ethan Wessel Tennen Studio 4702 East Indian School Road Phoenix, Arizona 85018

July 30, 2018

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Project 25998

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- 02 Oblique Aerial Photograph and Topographic Map
- 03 Site Plan
- 04 Main Slope Photographs
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THE SCOPE OF WORK FOR THIS REPORT MIRRORS THAT OF THE PROPOSAL AND IS AS FOLLOWS: 1) TWO (2) SEPARATE COMPLETE GEOMETRIES OF THE SLOPE WILL BE DRAWN. THE GEOMETRIES WILL INCLUDE THE TOE, ASPERITIES ALONG THE SLOPE FACE, SLOPE ANGLE, CHARACTER OF CREST, AND MEASUREMENT OF THE NATURAL UP SLOPE TERRAIN

2) SOIL AND ROCK TYPES ALONG THE GEOMETRY WILL BE EXAMINED, VERIFIED, AND PRESENTED **ON REPRESENTATIVE CROSS SECTION**

3) GEOLOGIC MEASUREMENTS OF DISCONTINUITIES WITHIN THE ROCK MASS WILL BE MADE. THESE WILL FOCUS ON FRACTURES AND FOLIATION ORIENTATION

4) BASED ON THE ABOVE, A KINEMATIC-LIKE ANALYSIS WILL BE PREFORMED SUING METHODOLOGIES ROCK ANCHORS CREATED BY MARKLAND. THESE ANALYSIS WILL DETERMINE THE POTENTIAL FOR PLANAR, WEDGE, AND TOPPLING FAILURES

5) A DETAILED DETERMINISTIC SLOPE STABILITY ANALYSIS WILL BE COMPLETED USING COMPUTER SOFTWARE KNOWN AS SLIDE

OBLIQUE AERIAL PHOTOGRAPH

- AT THE LOWEST FACTOR OF SAFETY FOR THE EXISTING SLOPE SECTIONS. FACTORS OF SAFETY **LESS THAN 1.5 WILL BE OF CONCERN**
- BE ASSIGNED A REMEDIAL ACTION MEASURE, RESULTING FROM EXHAUSTIVE COMPUTER MODELING TO ENSURE STABILITY
- 8) PHOTOGRAPHS AND DISCUSSION OF THE ROCK SLOPE ANALYZED 9) REMEDIAL RECOMMENDATIONS (IF NECESSARY) UTILIZING:

RETAINING WALLS MESH AND GROUT COMBINATION OF THE ABOVE

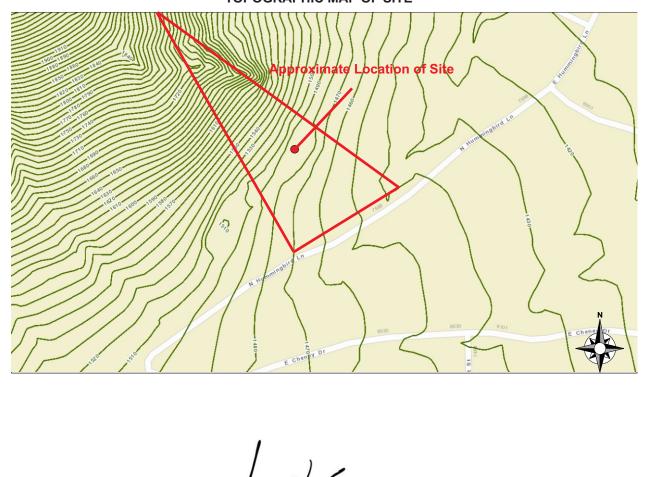
TOPOGRAPHIC MAP OF SITE



OBLIQUE AERIAL PHOTOGRAPH OF THE SITE, SHOWING THE CURRENT SITE CONDITIONS. THE EXISTING CUT SLOPE IS LOCATED ALONG THE WEST SIDE OF THE SITE SHOWN IN THE AERIAL PHOTOGRAPH (OUTLINED IN RED).

IT MUST BE NOTED THAT THIS REPORT AND THE RECOMMENDATIONS CONTAINED HEREIN ARE PREDICATED ON THREE REPORTS SERVING IN CONGRESS; 1) THIS REPORT, 2) THE GEOTECHNICAL INVESTIGATION REPORT DATED JULY 30, 2018, AND 3) THE BOULDER STABILITY EVALUATION REPORT DATED JULY 30, 2018. THIS REPORT IS, THEREFORE, A PORTION OF THE OVERALL STUDY OF THE SITE. BECAUSE OF THE UNIQUENESS OF EACH REPORT, THE CONTENTS ARE CONSTRAINED TO SEPARATE SUBMITTALS. NOTWITHSTANDING, ALL THREE REPORTS WILL WORK TOGETHER, ALL THREE REPORTS ARE IDENTIFIED BY THE PROJECT NUMBER 25998.





6) SEVERAL FAILURE MODES AND LOADS (INCLUDING SEISMIC SHAKING) WILL BE USED TO ARRIVE

7) BECAUSE OF THE ANALYSIS, ANY SLOPE SECTION WITH A FACTOR OF SAFETY LESS THAN 1.5 WILL

OBLIQUE AERIAL PHOTOGRAPH AND TOPOGRAPHIC MAP									
DATE: 7/30/18			REVIEWED BY: /ANN, MS PE D.GE F. ASCE						
PROPOSED CUSTOM HILLSIDE RESIDENCE APN 106-04-007 7550 NORTH HUMMINGBIRD LANE PARADISE VALLEY, ARIZONA									
PRO	JECT 25998								



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15206 JEFFRY D, GENERAL INFORMATION: 1) SLOPE HEIGHT (MAX): 16 FEET 2) GENERAL STRIKE: 10 DEGREES 3) MAX DIP: 80 DEGREES 4) DIP RANGE: 65-80 DEGREES 5) SLOPE STRUCTURE: HEAVILY BROKEN ROCK MASS

MAIN SLOPE: NORTH-NORTHEAST TO SOUTH-SOUTHWEST TRENDING CUT SLOPE; EAST-SOUTHEAST DIPPING; WEST SIDE OF PROPOSED BUILD AREA

		03
SITE PLAN		
DATE: 7/30/18	JEFFRY D.	REVIEWED BY: VANN, MS PE D.GE F. ASCE
PROPOSED CUSTOM HILLSID APN 169-04-007 7550 NORTH HUMMINGBI PARADISE VALLEY, AR		
PROJECT 25998		

1) FOLIATION OF CUT SLOPE

2) HEAVILY BROKEN ROCK MASS



FACING NORTH



FACING WEST





6) APPROXIMTE SLOPE ANGLE OF 65 DEGREES



FACING NORTH

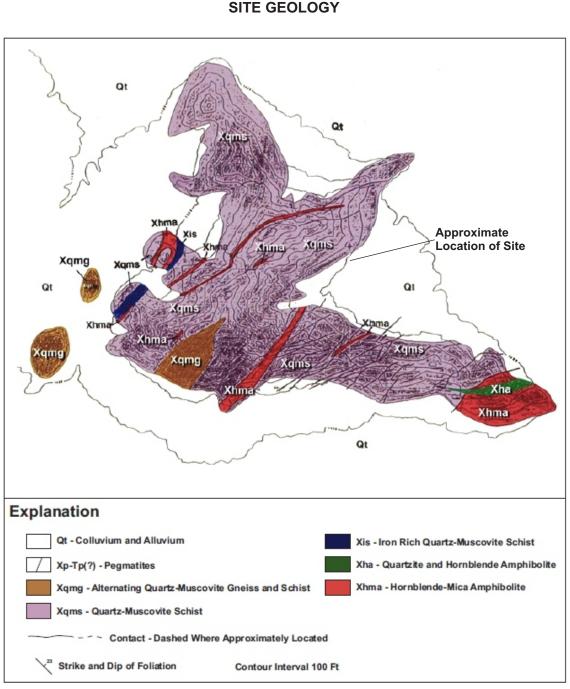
FACING WEST

3) CONJUGATE FRACTURE SET 1 4) CONJUGATE FRACTURE SET 2

5) APPROXIMTE SLOPE ANGLE OF 80 DEGREES

7) APPROXIMTE SLOPE ANGLE OF 65 DEGREES

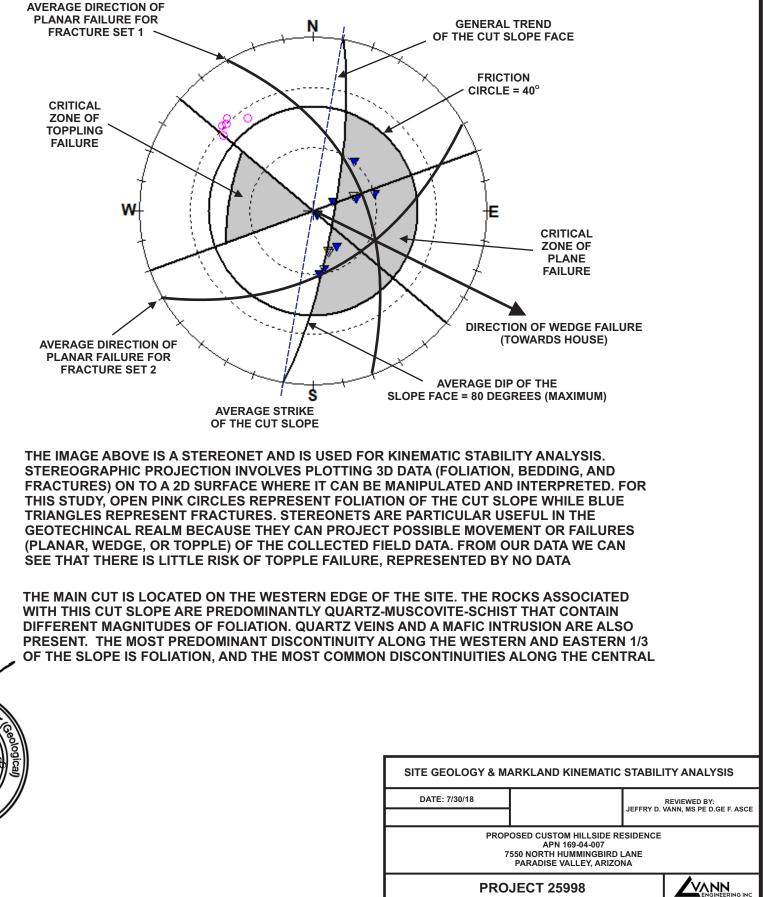
	MAIN SLOPE PHOTOGRAPHS	
DATE: 7/30/18		REVIEWED BY: JEFFRY D. VANN, MS PE D.GE F. ASCI
	PROPOSED CUSTOM HILLSIDE RESIDENCI APN 169-04-007 7550 NORTH HUMMINGBIRD LANE PARADISE VALLEY, ARIZONA	Ξ
	PROJECT 25998	



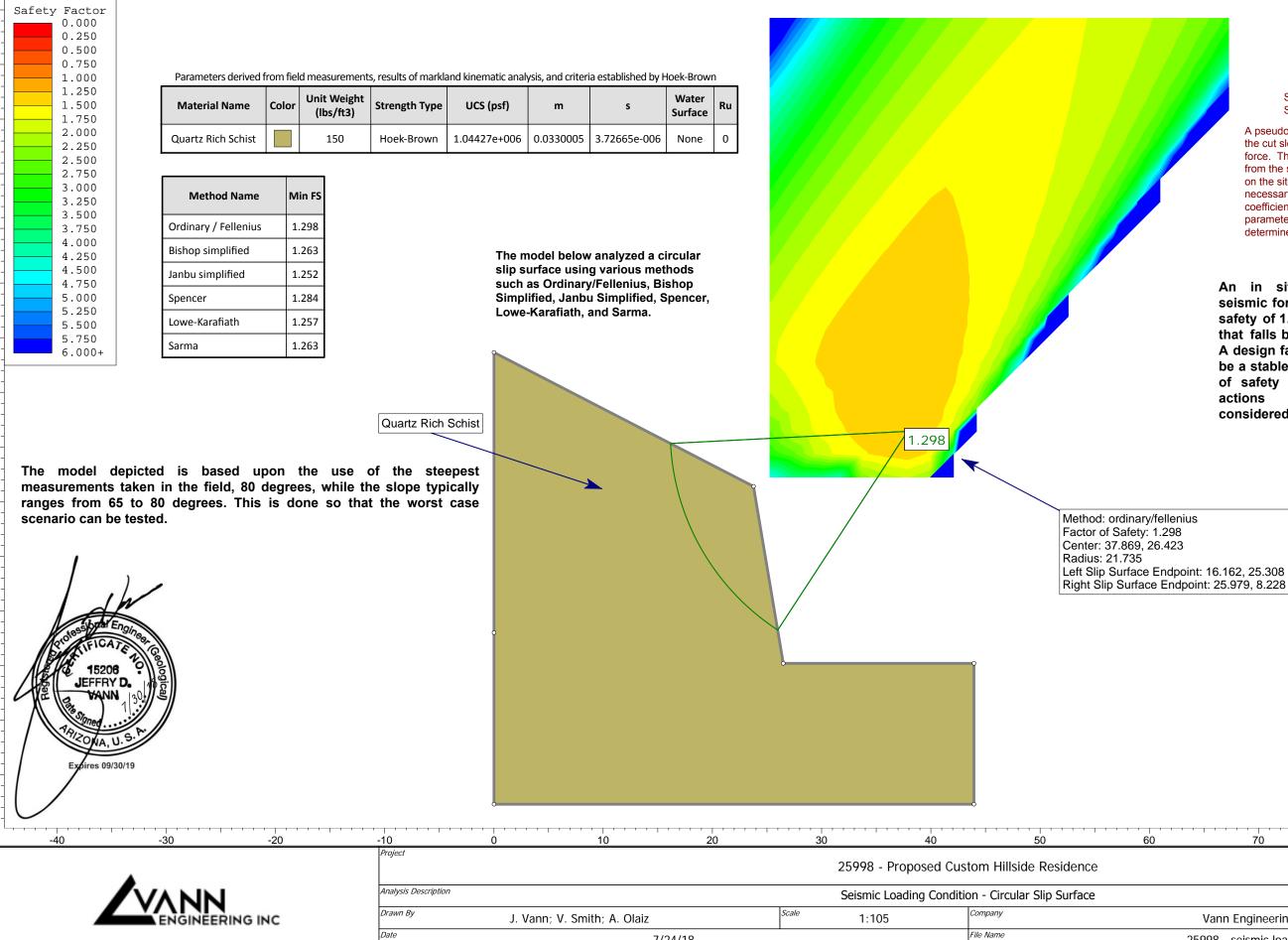
THE ROCK MASS THAT COMPRISES THE SITE IS PREDOMINANTLY QUARTZ -MUSCOVITE SCHIST (Xqms) THAT IS HIGHLY TO MODERATELY WEATHERED AND FRACTURED. REGIONALLY, THE STRIKE OF THE FOLIATION SOUTH OF THE SITE IS APPROXIMATELY 234° WITH A FOLIATION DIP OF 44° TO THE NORTHWEST. FURTHER, THE REGIONAL STRIKE OF THE FOLIATION WEST OF THE SITE IS APPROXIMATELY 228° WITH A DIP OF 27° TO THE NORTHWEST. BOTH SETS OF CONDITIONS SHOULD BE ANTICIPATED AT THE SITE. TO THE NORTH-NORTHWEST OF THE SITE, A PEGMATITE DIKE TRENDS FROM NORTH-NORTHEAST TO WEST-SOUTHWEST (DENOTED BY A SOLID LINE).

GEOLOGIC MAP REFERENCED FROM ARIZONA STATE UNIVERSITY LIBRARY, GEOLOGIC MAP OF MUMMY MOUNTAIN, BY AYLOR, J.G., 1973, MS THESIS, ARIZONA

MARKLAND KINEMATIC STABILITY ANALYSIS







7/24/18

DEINTERPRET 7.031

▶ 0.07 ٨w

Seismic Coefficient for Pseudo-Static Stability Analysis

A pseudo-static analysis approach is used to model the cut slopes response to an equivalent seismic force. The equivalent seismic force is determined from the site's seismic coefficient (ks), which is based on the site's earthquake history. The parameters necessary for the determination of the seismic coefficient are referenced from USGS. From these parameters, the site's seismic coefficient has been determined to be 0.07g.

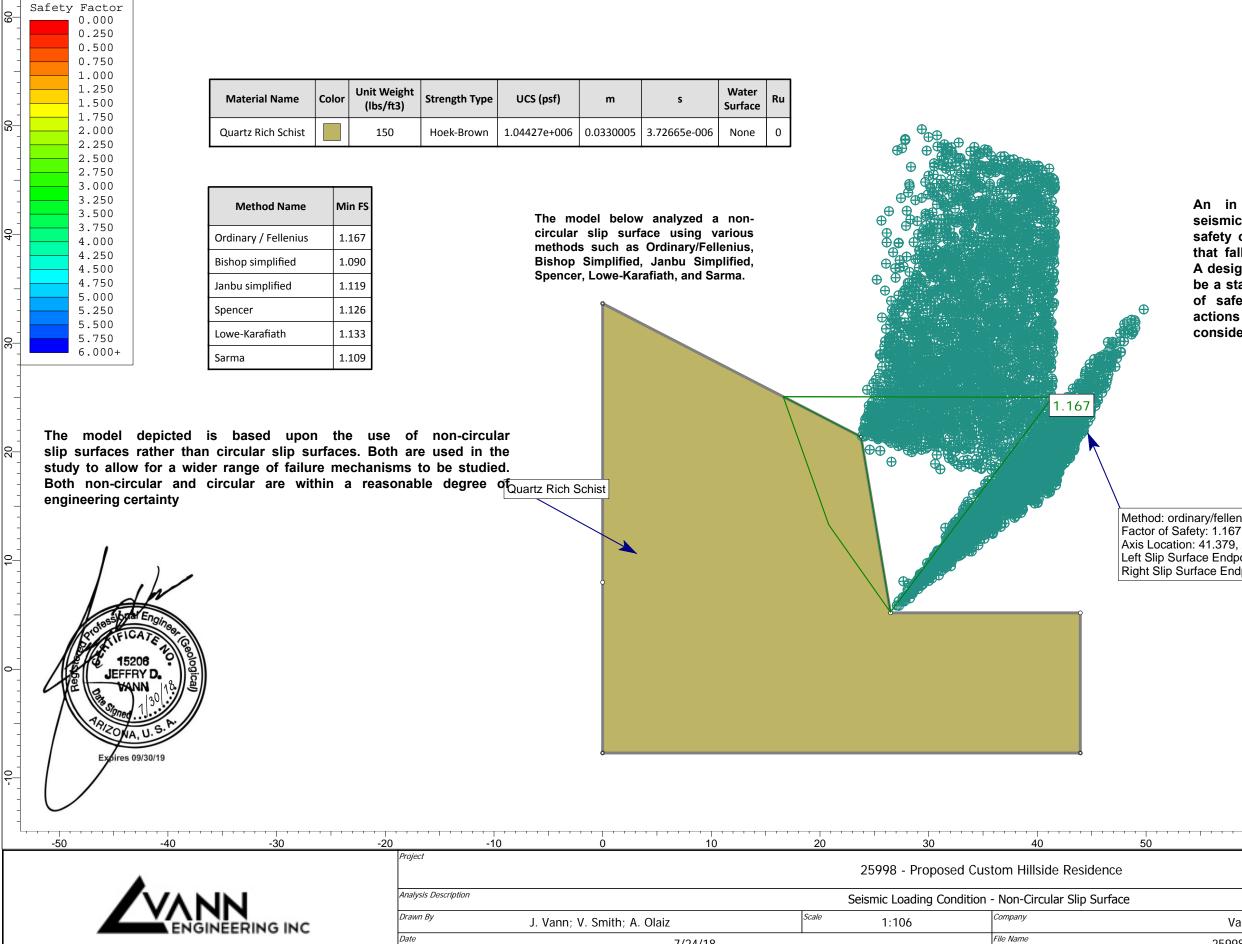
An in situ, with an applied site-specific seismic force, analysis resulting in a factor of safety of 1.298 indicates a potential for sliding that falls below a design factor of safety of 1.5. A design factor of safety of 1.5 is considered to be a stable slope. Therefore, because our factor of safety of 1.298 falls below 1.5, remedial actions such as bolting should be considered.

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7/24/18

Date

DEINTERPRET 7 031



Seismic Coefficient for Pseudo-Static Stability Analysis

An in situ, with an applied site-specific seismic force, analysis resulting in a factor of safety of 1.167 indicates a potential for sliding that falls below a design factor of safety of 1.5. A design factor of safety of 1.5 is considered to be a stable slope. Therefore, because our factor of safety of 1.167 falls below 1.5, remedial actions such as bolting should be considered.

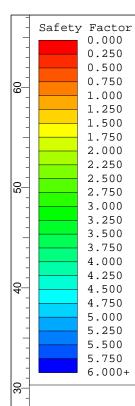
Method: ordinary/fellenius Axis Location: 41.379, 25.026 Left Slip Surface Endpoint: 16.614, 25.075 Right Slip Surface Endpoint: 26.481, 5.244

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15206

JEFFRY D.

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es 09/30/19

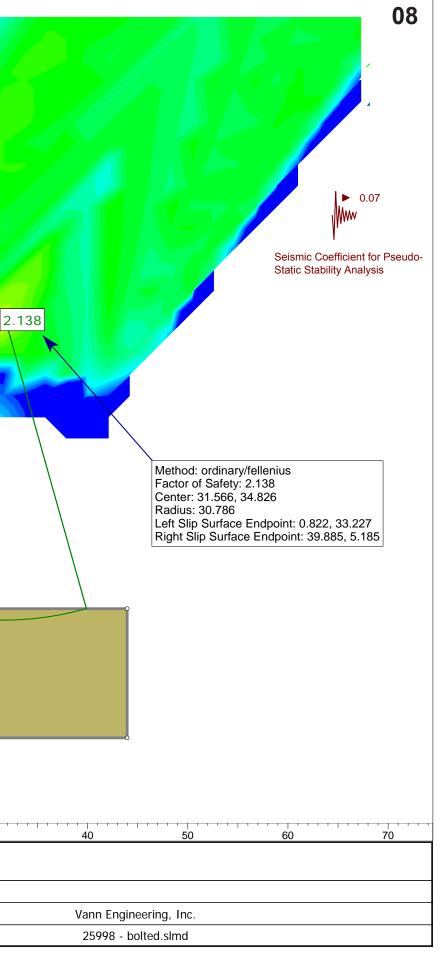
Support Name	Color	Ту	vpe Fo	orce A	Application	Out-Of-Plane Spacing (ft)	Tensile Capacity (lbs)	Plate Capacity (lbs)	Shear Cap (Ibs)		Compression Capacity (lbs)	Bond Length (ft)	Percent of Length (%)	Bond Strength (Ibs/ft)	Material Depender
Support 1			uted back A	ctive ((Method A)	6	79000	79000	0		0	0	60	5655	No
Material Name	e (Color	Unit We (Ibs/ft		Strength Typ	e UCS (psf) m	s	Water Surface	Ru					
Quartz Rich Schi	st		150		Hoek-Brown	n 1.04427e+(0.0330005	3.72665e-006	None	0					
Method Name	e	Min I	≓s												
Ordinary / Fellen	ius	2.13	8												
Bishop simplified	ł	2.35	3												
Janbu simplified		2.05	5												
Spencer		2.34	9												
Lowe-Karafiath		2.77	2									0			
Sarma		2.29	4												

In order to stabilize the slope and guard against a potential slope failure, rock bolting must be employed. With rock bolting, the Factor of Safety will increase above 2, with that Factor of Safety applicable only to the natural slope above the bolted portion. We recommend a bolt pattern of 6 feet by 6 feet across the slope. All measurements will be made along the slope face in a linear fashion. Both the upper and lower row of bolts will have 20-feet long bolts. We recommend the use of a 3 inch minimum diameter core hole.

> A bolted surface with an applied site-specific seismic force analysis resulting in a factor of safety of 2.138. When comparing the factor of safety with bolting (2.138) and without bolting (1.298 & 1.167), the recommended factor of safety of 1.5 is obtained when this bolting pattern is implemented. Furthermore, the minimum factor of safety results in the slip surface which daylights in the toe of slope, which for this type of rock has a very low probability of occurrence.

-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30			
			Project 25998 - Proposed Custom Hillside Residence											
					Analysis Description					Bolted Condition - Circular Slip Surface				
	ENG	NEERING IN	с	Drawn By	J. Vann; V	. Smith; A. Olaiz		Scale 1	1:115	Company				
SLIDEINTERPRET 7.031				Date		7/24	1/18	-		File Name				

Quartz Rich Schist



-	Safety	Factor
_		0.000
8–		0.250
-		0.500
-		0.750
		1.000
_		1.250
-		1.500
-		1.750
-		2.000
50		
2		2.250
_		2.500
-		2.750
-		3.000
_		3.250
		3.500
_		3.750
_		4.000
6–		4.250
-		4.500
-		4.750
_		5.000
-		5.250
-		5.500
-		5.750
0_		6.000+
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Support Name	Color	Туј	pe Force A	Application	Out-Of-Plane Spacing (ft)	Tensile Capacity (lbs)	Plate Capacity (lbs)	Shear Cap (lbs)		Compression Capacity (lbs)	Bond Length (ft)	Percent of Length (%)	Bond Strength (Ibs/ft)	Material Dependen
Support 1		Grou Tieb		(Method A)	6	79000	79000	0		0	0	60	5655	No
Material Nam	e (Color	Unit Weight (Ibs/ft3)	Strength Typ	e UCS (psf)	m	s	Water Surface	Ru					
Quartz Rich Sch	nist		150	Hoek-Browr	1.04427e+0	0.0330005	3.72665e-006	None	0					

In order to stabilize the slope and guard against a potential slope failure, rock bolting must be employed. With rock bolting, the Factor of Safety will increase above 2, with that Factor of Safety applicable only to the natural slope above the bolted portion. We recommend a bolt pattern of 6 feet by 6 feet across the slope. All measurements will be made along the slope face in a linear fashion. Both the upper and lower row of bolts will have 20-feet long bolts. We recommend the use of a 3 inch minimum diameter core hole.

3.013

3.189

3.147

3.139

3.387

Bishop simplified

Janbu simplified

Lowe-Karafiath

Spencer

Sarma

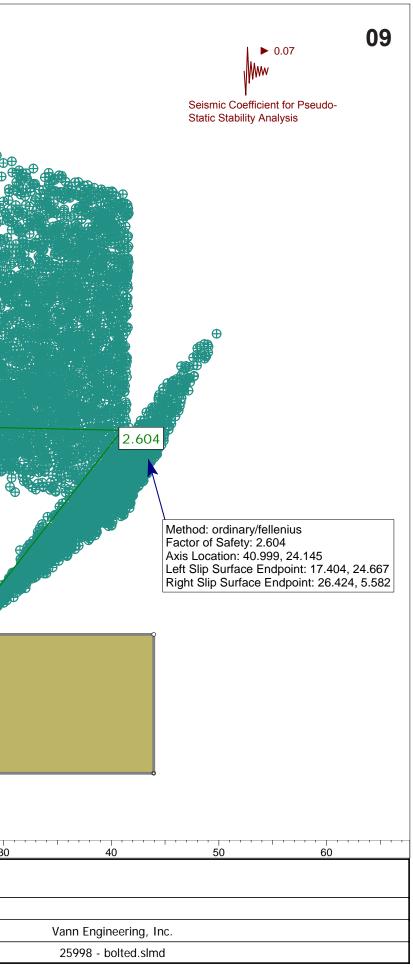
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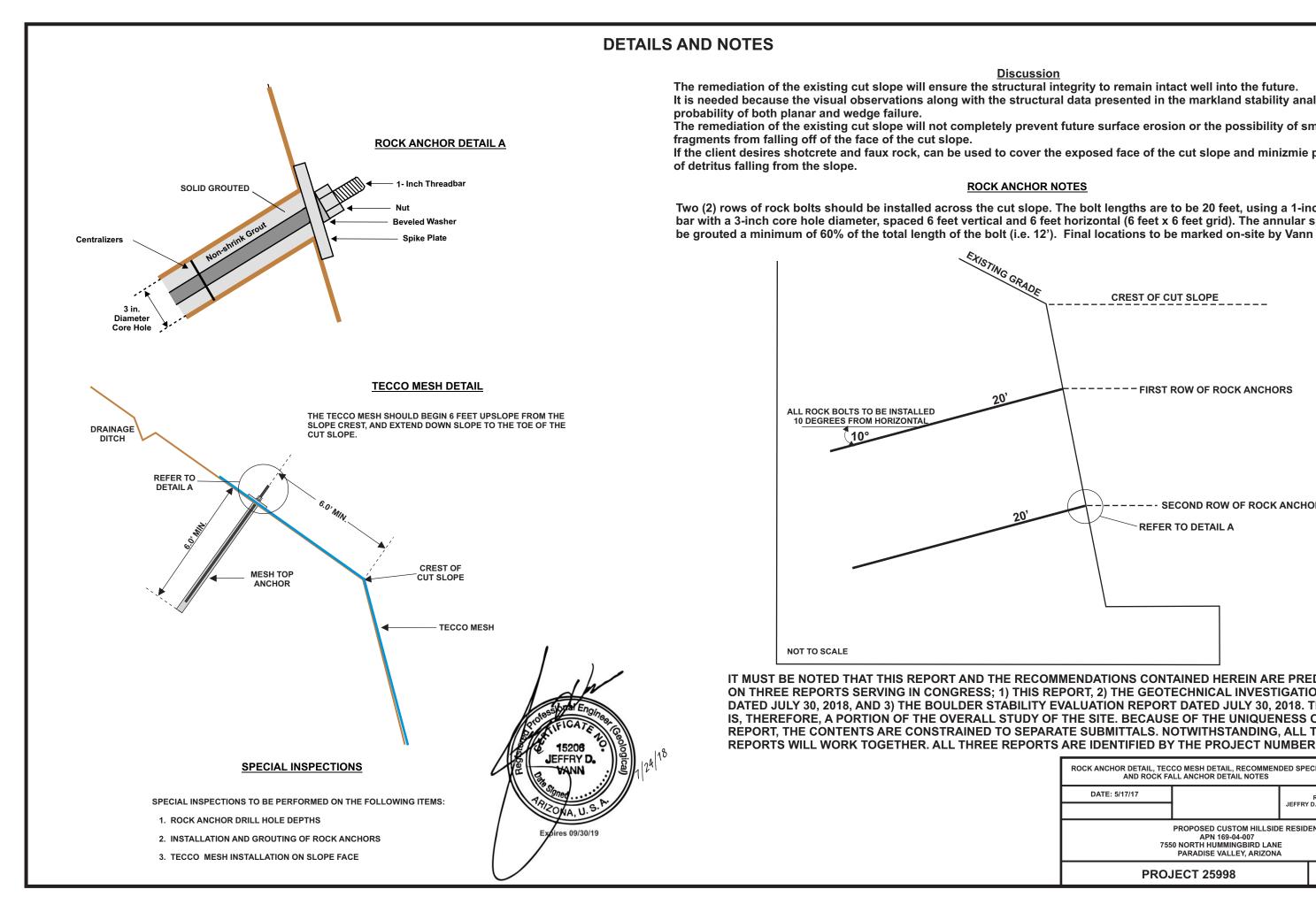
JEFFRY D.

es 09/30/19

A bolted surface with an applied site-specific seismic force analysis resulting in a factor of safety of 2.604. When comparing the factor of safety with bolting (2.604) and without bolting(1.298 & 1.167), the recommended factor of safety of 1.5 is obtained when this bolting pattern is implemented. Furthermore, the minimum factor of safety results in the slip surface which daylights in the toe of slope, which for this type of rock has a very low probability of occurrence. Quartz Rich Schist

-70	-60	-50	-40	-30	-20	-10	0	10	20	30
	Project		Proposed Custom H	posed Custom Hillside Residence						
			Analysis Description				Boltec	l Condition - Non-Circu	lar Slip Surface	
	NGINEERIN	G INC	Drawn By	J. Vann; V	Smith; A. Olaiz	Sca	^{le} 1:10	7 Company		
SLIDEINTERPRET 7.01			Date		7/24		File Name			
				Project Analysis Description Drawn By Date	Project Analysis Description Drawn By J. Vann; V. Date	Project Analysis Description Drawn By J. Vann; V. Smith; A. Olaiz Date 7/24	Project Analysis Description Drawn By J. Vann; V. Smith; A. Olaiz Date 7/24/18	Project 25998 - Analysis Description Boltect Drawn By J. Vann; V. Smith; A. Olaiz Scale 1:10 Date 7/24/18	Project 25998 - Proposed Custom H Analysis Description Bolted Condition - Non-Circu Drawn By J. Vann; V. Smith; A. Olaiz Scale 1:107 Company Date 7/24/18 File Name	Project 25998 - Proposed Custom Hillside Residence Analysis Description Bolted Condition - Non-Circular Slip Surface Drawn By J. Vann; V. Smith; A. Olaiz Scale 1:107 Company Date 7/24/18 File Name





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Discussion

It is needed because the visual observations along with the structural data presented in the markland stability analysis show a

The remediation of the existing cut slope will not completely prevent future surface erosion or the possibility of small rock

If the client desires shotcrete and faux rock, can be used to cover the exposed face of the cut slope and minizmie possibility

ROCK ANCHOR NOTES

Two (2) rows of rock bolts should be installed across the cut slope. The bolt lengths are to be 20 feet, using a 1-inch diameter bar with a 3-inch core hole diameter, spaced 6 feet vertical and 6 feet horizontal (6 feet x 6 feet grid). The annular space must

